



Numerical and stability analysis of Cu-Al₂O₃ water-based hybrid nanofluid through a permeable shrinking sheet: Multiple solutions

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Abstract

The aim of the current study is to investigate the numerical and theoretical analysis of a Hybrid Nanofluid (HNF) suspended with Cu and Al₂O₃ nanoparticles in water. The basic flow equations contain the influence of thermal radiation, magnetic field, temperature-dependent viscosity, cross-diffusion, and heat source. The basic flow equations described by Navier-Stokes have been altered to self-similar equations via transformations of variables. The transformed system is then solved numerically via the BVP4C approach. For stability exploration, the stability analysis is performed mathematically and graphically, which provides a novel contribution to the study. The impact of emerging factors on flow characteristics is elaborated through graphs. The present numerical results are correlated with the published work, and excellent agreement has been established. It is investigated that the velocity curves show a decreasing phenomenon due to the augmented values of variable viscosity and magnetic field. Opposite behavior is reported for the permeability factor, Grashof, and modified Grashof numbers. The fluid energy and concentration are increasing functions of the Dufour, Eckert, and Soret numbers.

1. Introduction

Mechanical performance and material choices are significantly impacted by the transmission of heat. In the fields of medical study, the mechanisms of metabolic heat production, blood transport, capillary dehydration, thermal management, and bio-heat exchanging routes make clear the significance of peristaltic fluid movement in heat transmission. All technological and biological structures generate heat, which causes a progressive decline in their ability to function. For such a device to function well, heat must be regularly evacuated from its construction. Novel materials having the ability to regulate heat transport are called Nanofluids (NFs). The process that is employed to turn regular fluids into NFs is called nanoprecipitation. Etemad et al. [1] looked at the turbulent dynamics of NFs with thermal convection analysis. Bég and Tripathi [2] elucidated the peristaltic flow caused by the cross-diffusion of NFs pursuant

to the influence of the Lorentz force. Bég et al. [3] analysed the NF in a permeable medium using an analytical technique. The computational models of NF across a vertical porous plate were provided by Rana et al. [4]. Convective boundary scenarios within a channel with porous walls have been used to find HAM-based conclusions for the NF Bég et al. [5]. The NF boundary layer mobility along an upward channel was explored by Rashidi et al. [6], and the method of homotopy analysis was used to get a quantitative result.

Hybrid Nanofluids (HNFs) are a novel and exciting class of aqueous fluids that have garnered a lot of interest since they can alter their thermophysical characteristics to boost heat transfer. This is achieved by mixing a number of nano-additives to fulfill the unique needs of every application. HNFs can be used in solar energy, electrical wiring, cooling structures, heat transfer devices, and heat tunnels.

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Muneeshwaran et al. [7] outlined the characteristics of HNFs in heat diffusion, although Kshirsagar and Venkatesh [8] described the wide range of technical uses for them. For solar systems, researchers have reported on the thermal and mixing features of HNFs [9,10]. Esfe et al. [11] anticipated that HNFs would be used in machining processes. Applications of HNFs with heat capacity were described by Adun et al. [12]. For the heat transfer rate, numerical findings were produced, and a visual representation of the physical components' influence on the flow field was provided. The HNFs were examined by Akilu et al. [13] to increase solar energy. In an analogous vein, Ashorynejad and Shahriari [14] examined the conduction of HNFs over a wavy cavity when Lorentz force was present.

Most investigations involving Magnetohydrodynamic (MHD) and NFs across stretched sheets typically include thermal fluidity or a constant wall temperature. Aziz [15] looked at the Blasius mobility across a stretched sheet under conduction heating conditions. Temimi et al. [16] studied the numerical solution for Troesh's problem using a Shishkin mesh. Ben-Romdhane and Temimi [17] reported the numerical solutions for the boundary layer problem. Falkner-Skan flow problem was discussed by Temimi and Ben-Romdhane [18]. Dual solutions for the 2D flow of Bratu's problem were displayed by Temimi and Ben-Romdhane [19].

Comparably, Chaudhary and Merkin looked into the magnetized NF using a warmed vertical plate [20]. Implications for chemical reactions have not been factored into these studies. Reaction is a crucial process in the processing of materials. The chemical reactions can be uniform, inconsistent, or endothermic. Kumar and Yadav [21] discussed the MHD movement with heat analysis of non-miscible micro polar fluid over a rectangular permeable sheet. Yadav and Yadav [22] investigated the heat and mass transmission of MHD couple-stress fluids over a permeable curved framework. Yadav and Srivastava [23] reported the influence of slip and permeable material in MHD movement across an inclined framework. Similarly, Jaiswal and Yadav [24] examined the movement of micropolar-Newtonian liquids with porous effect in a movable interface. Yadav et al. [25] reported the Poiseuille flow in a permeable pipe of micropolar Newtonian fluid. Boundary-layer convection formulations incorporating chemical processes have been distributed [26]. Manjunatha et al. [27] examined the effects of cross-diffusion and chemical processes on magnetized heat transfer. They discovered that chemical reaction ordering increases the concentrating boundary layer depth, but species diffusion increases the adverse chemical response rate.

The investigation of the stability of the time-dependent viscosity of HNFs over a stretching and contracting surface with the impact of heat radiation, chemical reactions, and cross-diffusion is novel in this work. This model is an extension of the models reported by Manjunatha et al. [27] and Venkateswarlu and Satya Narayana [28]. Moreover, stability analysis has been implemented, which has not been investigated yet. Through similarity variables, the fundamental flow model expressed by means of Partial Differential Equations (PDEs) is altered to a non-dimensional version expressed in systems of Ordinary Differential Equations (ODEs), and then solved numerically. The outcomes are validated against the available outcomes.

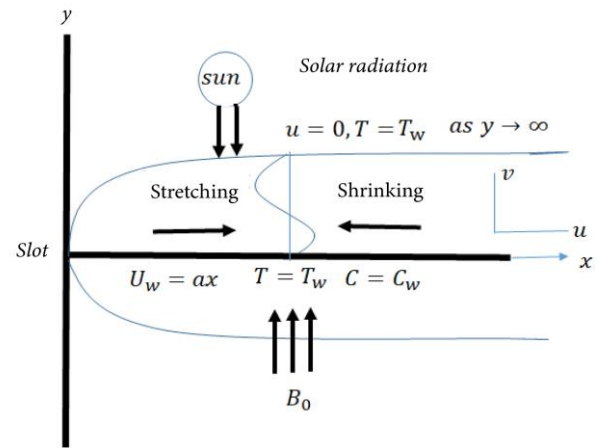


Figure1. Flow geometry.

The theoretical examination's results may soon find use in a wide range of industries, including the manufacture of medical equipment, surfactants, lubrication properties, hybrid power plants, solar heating and cooling technologies for automobiles, and metallurgical welding processes.

2. Mathematical analysis

In a porous medium comprising tiny particles of copper and alumina, the two-dimensional movement of HNFs is examined under the effects of heat radiation, chemical reactions, cross-diffusion, magnetic fields, and time-dependent viscosity. In this investigation, water is used as a host fluid. In Figure 1, the flow structure is illustrated. It is evident from the graphic that the flow is along the x -axis and the y -axis is normal to it. The extending/shrinking velocity is signified by $U_w = \lambda cx$, where λ is the stretching or shrinking parameter. The Lorentz force is applied normal to the flow. Here, T_w , T_∞ , C_w , and C signify the surface and ambient temperatures with surface, and ambient concentrations, respectively.

The leading flow equations of velocity, temperature, and concentration are given below B_0 .

$$\frac{\partial}{\partial x}(u) + \frac{\partial}{\partial y}(v) = 0, \quad (1)$$

$$\frac{1}{\rho_{hnf}} \left\{ \frac{\partial}{\partial y} \left(\mu_{hnf}(T) \frac{\partial u}{\partial y} \right) - \left(\sigma B_0^2 + \frac{\nu_f}{k_f} \right) u \right\} - \left\{ u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right\} + g \beta_{hnf} \{ (C - C_\infty) + (T - T_\infty) \} = 0, \quad (2)$$

$$\frac{1}{(\rho C p)_{hnf}} \left\{ \left(k_{hnf} + \frac{16\sigma^* T_\infty^3}{3k^*} \right) \frac{\partial^2 T}{\partial y^2} + Q^* (T - T_\infty) + QI^* (C - C_\infty) + \mu_{hnf} \left(\frac{\partial u}{\partial y} \right)^2 \right\} - \left\{ u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} \right\} + \frac{Dk_r}{CpC_s} \frac{\partial^2 C}{\partial y^2} = 0, \quad (3)$$

$$D_B \frac{\partial^2 C}{\partial y^2} - \left\{ u \frac{\partial C}{\partial x} + v \frac{\partial C}{\partial y} \right\} - K_r^* (C - C_\infty) + \frac{Dk_r}{T_m} \frac{\partial^2 T}{\partial y^2} = 0. \quad (4)$$

Table 1. Physical properties of H₂O, Al₂O₃, and Cu [27, 28].

Thermal physical properties	Al ₂ O ₃	Cu	Base fluid H ₂ O
Density (ρ)(kgm ⁻³)	3,9770	8,933	997.1
Thermal expansion coefficient ($\beta \times 10^{-5}$)(K ⁻¹)	5.1	76.5	25.6
Thermal conductivity (k)(Wm ⁻¹ K ⁻¹)	40	400	0.6071
Heat capacity (C_p)(Jkg ⁻¹ K ⁻¹)	765	385	4,179

With boundary conditions:

$$C = C_w, \quad T = T_w, \quad U_w = u = \lambda cx, \quad \text{and} \quad v = 0 \quad \text{at} \quad y = 0,$$

$$C = C_\infty, \quad T = T_\infty, \quad u = 0, \quad \text{and} \quad v = 0 \quad \text{at} \quad y \rightarrow \infty. \quad (5)$$

Tables 1 and 2 signify the thermo-physical properties of the proposed model,

$$\text{where} \quad \frac{k_{bf}}{k_f} = \frac{k_{s1} + (n-1)\{k_f + \phi_2(k_{s1} - k_f)\}}{k_{s1} + (n-1)\{k_f + \phi_2(k_f - k_{s1})\}},$$

for time-dependent viscosity, the following relation is used [27,29]:

$$\mu_f = \mu_0 e^{-B\theta(\eta)}. \quad (6)$$

The term $e^{-B\theta(\eta)}$ can be expand by utilizing Maclaurin's series:

$$e^{-B\theta} = 1 - (B\theta) + O(B^2). \quad (7)$$

In terms of variable viscosity, HNFs is reported as:

$$\begin{aligned} & \frac{\mu_f}{(1-\phi_1)^{2.5}(1-\phi_2)^{2.5}}, \\ \mu_{hmf}(T) &= \frac{\mu_0}{(1-\phi_1)^{2.5}(1-\phi_2)^{2.5}} \exp\{1 - B\theta(\eta)\}, \\ & \frac{\mu_0}{(1-\phi_1)^{2.5}(1-\phi_2)^{2.5}} \exp\{1 - (B\theta) + O(B^2)\}. \end{aligned} \quad (8)$$

In Eq. (8), B (for liquid ($B < 0$), for gases ($B > 0$) is a parameter depending on the viscosity of the fluid, and μ_0 is the reference viscosity.

Using the transformation variable [27,28]:

$$\begin{aligned} u &= axf'(\eta), \quad v = -\sqrt{a\nu_f}f(\eta), \quad \theta(\eta) = \frac{T_\infty - T}{T_\infty - T_w}, \\ \varphi(\eta) &= \frac{C_\infty - C}{C_\infty - C_w}, \quad \eta = \sqrt{\frac{a}{\nu_f}}y, \end{aligned} \quad (9)$$

In view of Eq. (9), Eqs. (2)-(5) become:

$$\begin{aligned} (1-B\theta)f'' - A_2A_1(f'^2 - f''f) + A_3A_2A_1(Gm\varphi + Gr\theta) \\ - Bf''\theta' - A_1(1/K + M)f' = 0, \end{aligned} \quad (10)$$

$$\begin{aligned} \frac{1}{Pr} \left\{ A_3 + \frac{4}{3}R \right\} \theta'' + A_4f\theta' + Q\theta + Ql\phi \\ + A_1A_3Ec f'^2 + A_4Du\phi'' = 0, \end{aligned} \quad (11)$$

$$\frac{1}{Sc} \varphi'' + f\varphi' - Kr\varphi + Sr\theta' = 0, \quad (12)$$

with:

$$\begin{aligned} f' = \lambda, \quad \theta = 1, \quad \phi = 1, \quad f = 0 \quad \text{at} \quad \eta = 0, \\ f' = 0, \quad \theta = 0, \quad \phi = 0 \quad \text{at} \quad \eta \rightarrow \infty. \end{aligned} \quad (13)$$

In above equations the parameters are given below:

$$\begin{aligned} Gr &= \frac{g\beta_f(T_w - T_\infty)}{aU_w}, \quad Gm = \frac{g\beta_f(C_w - C_\infty)}{aU_w}, \quad K = \frac{a(k\rho)_f}{\nu_f}, \\ Kr &= \frac{Kr^*}{a}, \quad M = \frac{\sigma B_0^2}{a\rho_f}, \quad Ec = \frac{u_w^2}{(C_p)_f(T_w - T_\infty)}, \quad Pr = \frac{\nu_f(\rho Cp)_f}{k_f}, \\ R &= \frac{4\sigma^*T_\infty^3}{k^*k_f}, \quad Q = \frac{Q^*}{a(\rho Cp)_f}, \quad Sc = \frac{\nu_f}{D_B}, \quad Sr = \frac{Dk_f}{T_n\nu_f} \left(\frac{T_w - T_\infty}{C_w - C_\infty} \right), \\ u &= \frac{Dk_f}{C_pC_s\nu_f} \left(\frac{C_w - C_\infty}{T_w - T_\infty} \right), \quad Ql = \frac{Ql^*}{a(\rho Cp)_f} \left(\frac{C_w - C_\infty}{T_w - T_\infty} \right). \end{aligned}$$

Dimensionless Local Skin Friction and Local Nusselt number are:

$$\begin{aligned} S_f Re_x^{\frac{1}{2}} &= -\frac{\mu_{hmf}}{\mu_f} f''(0), \\ N_n^{-\frac{1}{2}} &= -\frac{K_{hmf}}{K_f} \theta'(0). \end{aligned}$$

3. Numerical solution

Nonlinear ODEs (10)–(12) with Constraint (13) cannot be analytically addressed. Computational methods are required to solve differential equations of this type. Although the available literature presents several numerical techniques, the BVP4C technique is mostly helpful for 1st-order Initial Value Problem (IVP). Consequently, we solved the System (10)–(12) using the BVP4C method and the relevant Constraint (13). The aforementioned equations are changed to a system of 1st-order by employing the alteration variables:

$$\begin{aligned} f &= f_1, \quad \frac{df}{d\eta} = f' = f_2, \quad \frac{d^2f}{d\eta^2} = f'' = f_3, \quad \theta = f_4, \\ \frac{d\theta}{d\eta} &= \theta' = f_5, \quad \phi = f_6, \quad \frac{d\phi}{d\eta} = \phi' = f_7. \end{aligned} \quad (14)$$

Using (14) in (10)–(13), we have:

$$f_3' = \frac{1}{1-B\theta} \left\{ A_1A_2 \left\{ (f_2^2 - f_1f_3) - A_3(Gmf_6 + Grf_4) \right\} + Bf_3f_5 + A_1 \left(\frac{1}{K} + M \right) f_2 \right\}, \quad (15)$$

$$\begin{aligned} f_5' &= -E^* \\ \{A_4f_1f_5 + Qf_4 + Qlf_6 + A_1Ec f_3'^2 + A_4DuSc(Kr f_6 - f_1f_7)\} & \end{aligned} \quad (16)$$

$$f_7' = -F^* \left\{ f_1f_7 - Kr f_6 - \frac{3PrSr}{A_3 + 4R} \{A_4f_1f_5 + Qf_4 + Qlf_6 + A_1Ec f_3'^2\} \right\}. \quad (17)$$

Corresponding to the conditions:

Table 2. Thermo-physical properties of Hybrid Nanofluids (HNFs) and NFs [27, 28].

Thermal physical properties	HNFs (Cu – Al ₂ O ₃ : H ₂ O)	NFs (Cu: H ₂ O)
μ	$\mu_{hnf} = \mu_f(1 - \phi_1)^{-2.5}(1 - \phi_2)^{-2.5}$	$\mu_{nf} = \mu_f(1 - \phi_2)^{-2.5}$
ρ	$\rho_{hnf} = \phi_2\rho_{s2}\{(1 - \phi_1)\rho_f + \phi_1\rho_{s1}\} + \phi_2\rho_{s2}$	$\rho_{nf} = (1 - \phi_2)\rho_f + \phi_2\rho_{s2}$
β	$\beta_{hnf} = \phi_2\beta_{s2}\{(1 - \phi_1)\beta_f + \phi_1\beta_{s1}\} + \phi_2\beta_{s2}$	$\beta_{nf} = (1 - \phi_2)\beta_f + \phi_2\beta_{s2}$
C_p	$(\rho C_p)_{hnf} = \phi_2(\rho C_p)_{s2} + (1 - \phi_2)(\rho C_p)_{s2}$ $\{(1 - \phi_1)(\rho C_p)_f + \phi_1(\rho C_p)_{s1}\}$	$(\rho C_p)_{nf} = (1 - \phi_2)(\rho C_p)_f + \phi_2(\rho C_p)_{s2}$
k	$\frac{k_{hnf}}{k_{bf}} = \frac{k_{s1} + (n - 1)\{k_{hf} + \phi_1(k_{s1} - k_f)\}}{k_{s1} + (n - 1)\{k_{bf} + \phi_1(k_f - k_{s1})\}}$	$\frac{k_{nf}}{k_f} = \frac{k_{s2} + (n - 1)\{k_f + \phi_2(k_{s2} - k_f)\}}{k_{s2} + (n - 1)\{k_f + \phi_2(k_f - k_{s2})\}}$

$$\begin{aligned} f_{1a^*} &= 0, & f_{2a^*} &= \lambda, & f_{4a^*} &= 1, & f_{6a^*} &= 1, \\ f_{2b^*} &= \lambda, & f_{4b^*} &= 1, & f_{6b^*} &= 1, \end{aligned} \quad (18)$$

where,

$$E^* = -\frac{3Pr}{3A_5 + 4R - 3A_4PrDuScSr},$$

$$F^* = -\frac{(A_5 + 4R)Sr}{A_5 + 4R - A_4DuPrSCSr}.$$

The set of Eqs. (15)–(17) and the associated boundary conditions provided by Eq. (18) can be addressed using the BVP4C method. Until the solution satisfies the convergence requirements, the process is repeated to confirm that the results satisfy the necessary accuracy level of 10^{-6} . In Figure 2, the BVP4C structure is shown.

4. Stability analysis

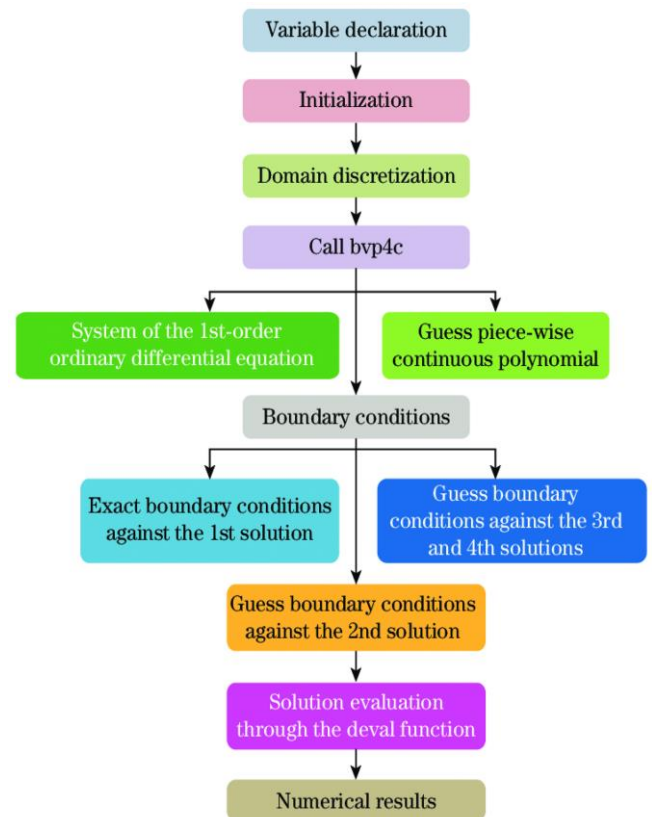
Together with the shooting procedure, the resultant nonlinear ODEs are computed using the BVP4C method. For the purposes of this investigation, stability analysis is used since certain values show dual solutions. Stretching or shrinking the sheet leads to dual solutions. For this reason, finding a stable and physically possible stability analysis of the problem is important. The approach used for stability analysis is precisely the same as that described by Dero et al. [30]. The unsteady flow equations are:

$$\frac{\partial}{\partial x}(u) + \frac{\partial}{\partial y}(v) = 0, \quad (19)$$

$$\begin{aligned} \frac{\partial u}{\partial t} + \frac{1}{\rho_{hnf}} \left\{ \frac{\partial}{\partial y} \left(\mu_{hnf}(T) \frac{\partial u}{\partial y} \right) - \left(\sigma B_0^2 + \frac{v_f}{k_f} \right) u \right\} \\ - \left\{ u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right\} + g\beta_{hnf} \{(C - C_\infty) + (T - T_\infty)\} = 0, \end{aligned} \quad (20)$$

$$\begin{aligned} \frac{\partial T}{\partial t} + \frac{1}{(\rho C_p)_{hnf}} \left\{ (k_{hnf} + \frac{16\sigma^* T_\infty^3}{3k^*}) \frac{\partial^2 T}{\partial y^2} + Q^*(T - T_\infty) + QI^*(C - C_\infty) \right. \\ \left. + \mu_{hnf} \left(\frac{\partial u}{\partial y} \right)^2 \right\} - \left\{ u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} \right\} + \frac{Dk_T}{CpC_s} \frac{\partial^2 C}{\partial y^2} = 0. \end{aligned} \quad (21)$$

$$\frac{\partial C}{\partial t} + D_B \frac{\partial^2 C}{\partial y^2} - \left\{ u \frac{\partial C}{\partial x} + v \frac{\partial C}{\partial y} \right\}$$

**Figure 2.** BVP4C procedure.

$$-K_r^*(C - C_\infty) + \frac{Dk_T}{T_m} \frac{\partial^2 T}{\partial y^2} = 0. \quad (22)$$

The corresponding boundary conditions are:

$$\begin{aligned} C = C_w, \quad T = T_w, \quad U_w = u = \lambda cx, \quad \text{and} \quad v = 0 \quad \text{at} \quad y = 0, \\ C = C_\infty, \quad T = T_\infty, \quad u = 0, \quad \text{and} \quad v = 0 \quad \text{at} \quad y \rightarrow \infty. \end{aligned} \quad (23)$$

According to Dero et al. [30], the subsequent alterations of variables are presented to convert the unsteady PDEs (20)–(23) in terms of ODEs.

Using the transformation variable [30].

$$\begin{aligned} u(x, t) &= axf'(\eta, \Gamma), & v(x, t) &= -\sqrt{a^*v_f} f(\eta, \Gamma), \\ \theta(x, t) &= \frac{T_\infty - T}{T_\infty - T_w}, & \phi(x, t) &= \frac{C_\infty - C}{C_\infty - C_w}, \end{aligned}$$

Table 3. Validation table for Surface Drag Force (SDF) [27,28].

M & B	SDF					
	[27]		[28]		Recent study	
	Cu – H ₂ O	Cu – Al ₂ O ₃ – H ₂ O	Cu – H ₂ O	Cu – Al ₂ O ₃ – H ₂ O	Cu – H ₂ O	Cu – Al ₂ O ₃ – H ₂ O
0.3	0.5070	0.5005	0.50714	0.50142	0.507107	0.500426
0.6	0.5545	0.5584	0.55467	0.55930	0.554603	0.558382
0.9	0.6010	0.6142	0.60112	0.61518	0.601160	0.614102
1.5	0.6465	0.6680	0.64664	0.66894	0.646665	0.668310
2.0	0.6910	0.7199	0.69217	0.72925	0.691100	0.719205
2.5	0.7504	0.7961	0.75192	0.81063	0.7501031	0.796038
3.0	0.8146	0.8794	0.81665	0.90014	0.814503	0.879341
3.5	0.8838	0.9699	0.88641	0.99762	0.883514	0.968826

Table 4. Validation table for Nusselt number using various quantities of Pr.

Pr	Nusselt number (Nn)					
	[27]		[28]		Recent study	
	Cu – H ₂ O	Cu – Al ₂ O ₃ – H ₂ O	Cu – H ₂ O	Cu – Al ₂ O ₃ – H ₂ O	Cu – H ₂ O	Cu – Al ₂ O ₃ – H ₂ O
0.7	0.2037	0.2064	0.20198	0.20582	0.203620	0.206261
1.2	0.2014	0.2128	0.20185	0.21694	0.201372	0.215536
1.5	0.2021	0.2192	0.20273	0.21885	0.202174	0.218904
2.2	0.2027	0.2257	0.20269	0.22727	0.203053	0.226425

$$\eta = \sqrt{\frac{a}{\nu_f}} y, \quad \Gamma = ct. \quad (24)$$

In view of Eq. (24), Eqs. (20)-(23) become:

$$(1-B\theta) \frac{\partial^3 f}{\partial \eta^3} - A_2 A_1 \left(\left(\frac{\partial f}{\partial \eta} \right)^2 - \frac{\partial^2 f}{\partial \eta^2} f \right) + A_3 A_2 A_1 (Gm\phi + Gr\theta) - B \frac{\partial^2 f}{\partial \eta^2} \frac{\partial \theta}{\partial \eta} - A_1 \left(\frac{1}{K} + M \right) \frac{\partial f}{\partial \eta} - \frac{\partial^2 f}{\partial \eta \partial \Gamma} = 0, \quad (25)$$

$$\frac{1}{Pr} \left\{ A_5 + \frac{4}{3} R \right\} \frac{\partial^2 \theta}{\partial \eta^2} + A_4 f \frac{\partial \theta}{\partial \eta} + Q\theta + Ql\phi + A_4 Ec \left(\frac{\partial^2 f}{\partial \eta^2} \right)^2 + A_4 Du \frac{\partial^2 \phi}{\partial \eta^2} - \frac{\partial^2 \theta}{\partial \eta \partial \Gamma} = 0, \quad (26)$$

$$\frac{1}{Sc} \frac{\partial^2 \phi}{\partial \eta^2} + f \frac{\partial \phi}{\partial \eta} - Kr\phi + Sr \frac{\partial \theta}{\partial \eta} - \frac{\partial \phi}{\partial \Gamma} = 0. \quad (27)$$

With:

$$\begin{aligned} \frac{\partial f}{\partial \eta}(\eta=0, \Gamma) &= \lambda, & \frac{\partial f}{\partial \eta}(\eta \rightarrow \infty, \Gamma) &= 0, \\ \theta(\eta \rightarrow \infty, \Gamma) &= 0, & \phi(\eta \rightarrow \infty, \Gamma) &= 0. \end{aligned} \quad (28)$$

Referring to Lund et al. [29], the reliability of the steady movement can be observed where

$$f_0(\eta) = f(\eta), \theta_0(\eta) = \theta(\eta) \text{ and } \phi_0(\eta) = \phi(\eta)$$

which satisfy (10)-(13), i.e.,

$$f(\eta, \Gamma) = f_0(\eta) + e^{-\gamma \Gamma} J(\eta, \Gamma),$$

$$\theta(\eta, \Gamma) = \theta_0(\eta) + e^{-\gamma \Gamma} F(\eta, \Gamma),$$

$$\phi(\eta, \Gamma) = \phi_0(\eta) + e^{-\gamma \Gamma} G(\eta, \Gamma), \quad (29)$$

where $F(\eta)$, $J(\eta)$, and $G(\eta)$, are relatively small to $f_0(\eta)$, $\theta_0(\eta)$, and $\phi_0(\eta)$ and γ is the eigenvalue (unknown). In view of (29), Eqs. (25)-(27), and taking $\Gamma = 0$.

$$(1-B\theta)J'' - A_2 A_1 (J'^2 - J' f_0) + A_3 A_2 A_1 (Gm\phi + Gr\theta) - BJ'F' - A_1 (1/K + M)J' + \gamma J = 0, \quad (30)$$

$$\frac{1}{Pr} \left\{ A_5 + \frac{4}{3} R \right\} F' + A_4 f_0 F' + Q\theta_0 + Ql\phi_0 + A_4 Ec J'^2 + A_4 Du G'' + \gamma F = 0, \quad (31)$$

$$\frac{1}{Sc} G'' + f_0 G' - Kr\phi_0 + SrF' = 0. \quad (32)$$

With,

$$\begin{aligned} J' &= \lambda, \quad F = 1, \quad G = 1, \quad J = 0 \quad \text{at} \quad \eta = 0, \\ J' &= 0, \quad F = 0, \quad G = 0 \quad \text{at} \quad \eta \rightarrow \infty. \end{aligned} \quad (33)$$

According to [29,30]. So, $J' = 0$ at $\eta \rightarrow \infty$ will be taken as $J''(0) = 1$.

5. Results and discussion

In this section, we shall examine the intriguing effects of several physical parameters of interest on flow dynamics. Additionally, we will discuss the engineering properties of mass movement rates, heat, and SF that are present in both conventional and HNFs streams over a perforated sheet. The complicated set of Problems (13)–(15) is solved numerically using the BVP4C approach, along with boundary Conditions (16), and represented graphically.

The present investigated results are confirmed by comparing with the published study, as shown in Tables 3 and 4. Tables 3 and 4 show that when $R = Q = Ql = 0 = Du = Sc = Sr = Kr$, there is a strong correlation between the present findings and published [27,28] for different values of $Ec = 0:3$

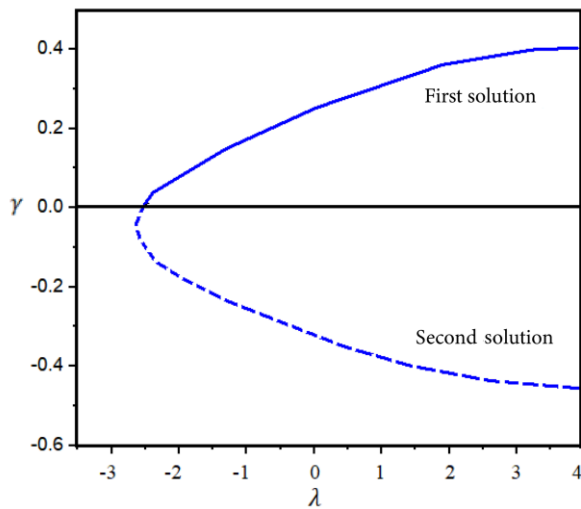


Figure 3. Stable and unstable solutions presentation.

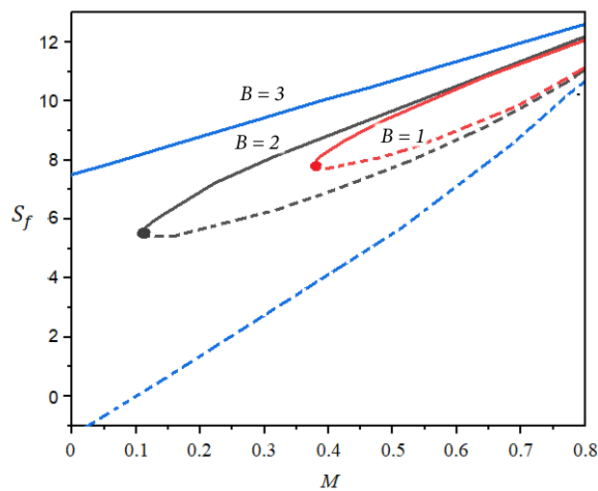


Figure 4. Scattering of S_f regarding B and M .

$Pr=0.5$, and $Gr = B = 1.2$. Furthermore, it is clear from the table that as parameters M , B , and Pr grow, so do the SDF and Nusselt number. Moreover, it is noteworthy that SDF and heat transfer for $Cu-Al_2O_3-H_2O$ is higher than $Cu-H_2O$.

Theoretical and visual stability explorations are offered to determine the stable configuration that results from the contracting sheet. Figure 3 provides a graphical representation of the dual solutions. According to Dero et al. [30], a solution is stable for positive eigenvalues and unstable for negative. The crucial point represents convergence, where the 1st and 2nd branches meet. When there are several branches, the stability examination is heavily used to assess the stable branch.

The impact of B (variable viscosity factor), M (magnetic factor), Gr (Grashof number), Du (Dufour number), Ec , (Eckert number), Q (heat source) and Ql (radiation absorption) on the skin friction (S_f) and Nusselt number (N_n) is illustrated in Figures 4–10. Figures 4–6 demonstrate the changes in S_f for various values of B , M , and Gr , while Figures 7–10 scrutinize the influence of Du , Ec , Q , and Ql on the fluctuation of (S_f). In Figure 4, it is depicted that as the amount of B and M increases, the value of S_f also increases. Notably, the parameters B and M exhibit dual fluctuation on (S_f). In the first branch, (S_f) experiences an increase, whereas

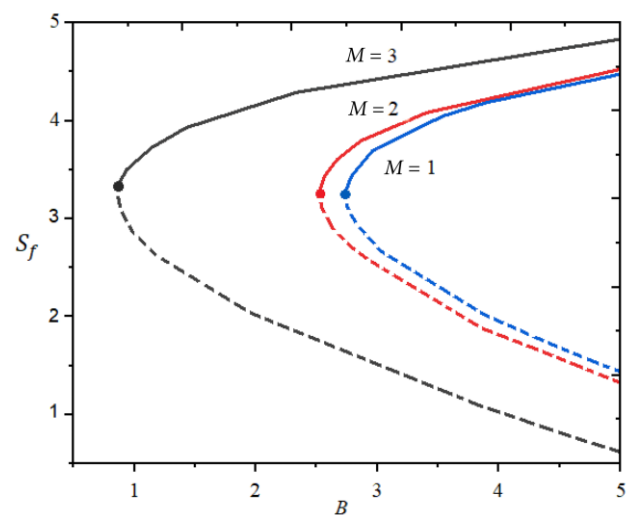


Figure 5. Scattering of S_f regarding M and B .

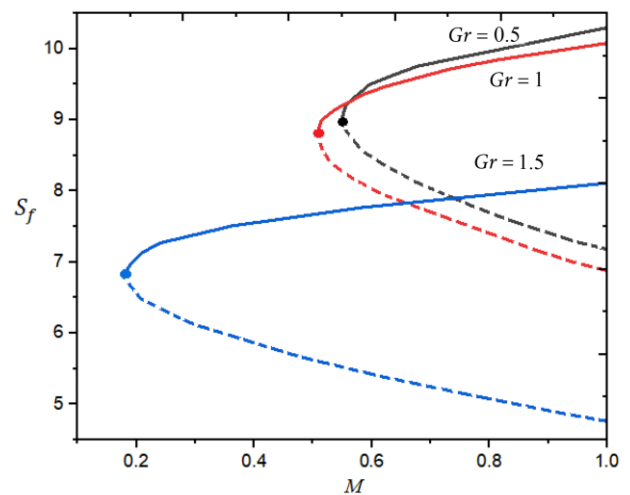


Figure 6. Scattering of S_f regarding M and Gr .

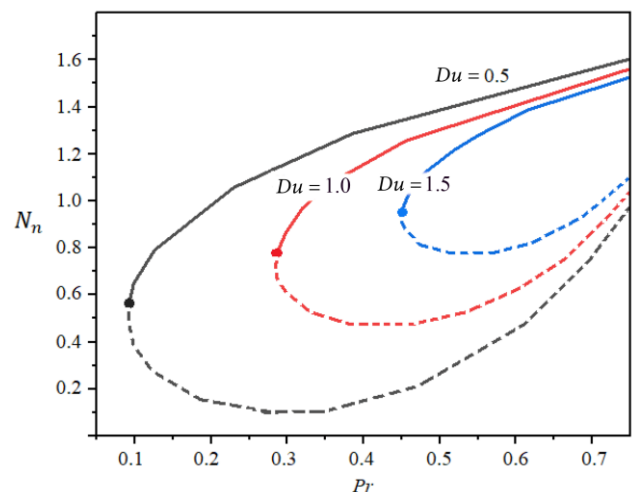


Figure 7. Distribution of N_n regarding Du and Pr .

in the second branch, (S_f) witnesses a decrease. This phenomenon can be ascribed to the presence of the Lorentz force, which arises from the magnetic field and opposes the flow, resulting in a decline in (S_f) during the second branch. The disparity in the amount of M in the variation of (S_f) is

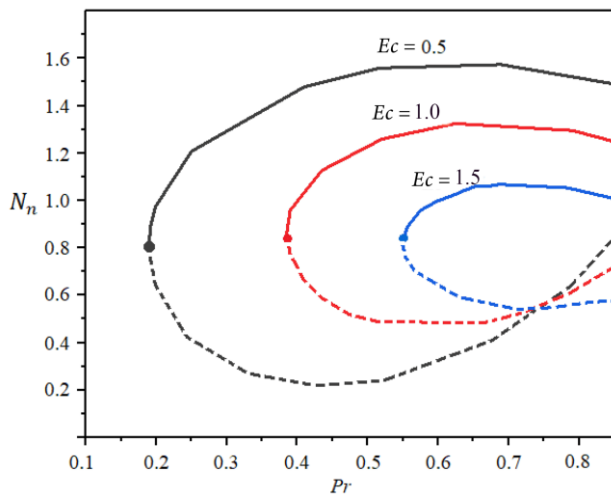


Figure 8. Distribution of N_n regarding Ec and Pr .

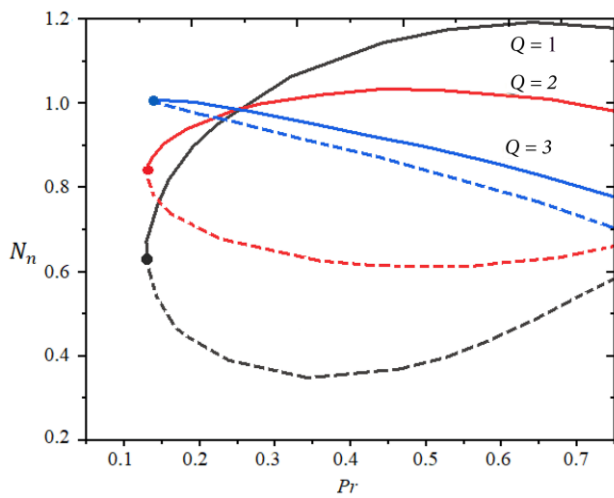


Figure 9. Distribution of N_n regarding Q and Pr .

shown in Figure 5. The data reveals that as M increases from 1 to 3, (S_f) experiences an enhancement.

Similarly, as the value of B increases from 1 to 5, the parameter S also experiences a corresponding increase. The rise in S can be directly attributed to the increasing magnitudes of M , which range from 1 to 3. The reason behind this phenomenon lies in the resistive forces becoming more prominent and discernible within this range. The mixture of Cu and alumina nanoparticles known as HNFs, plays a crucial role in promoting an enhanced resistance to movement. This is primarily due to the higher surface area possessed by these nanoparticles and their amplified interaction with the liquid component.

The influence of Gr and M on (S_f) of HNFs is illustrated in Figure 6. Interestingly, a dual behavior is observed in relation to these parameters. The term Gr pertains to the buoyancy forces involved in the fluid drive. Upon investigation, it is found that the value of (S_f) drops as the values of Gr and M are improved. This implies that as Gr and M values increase, the skin friction experienced by HNFs decreases.

The occurrence of this inverse behavior can be attributed to the low resistance encountered during the movement, which can be primarily attributed to the increasing values of Gr . The rising level of Gr introduces a resilient fluid motion,

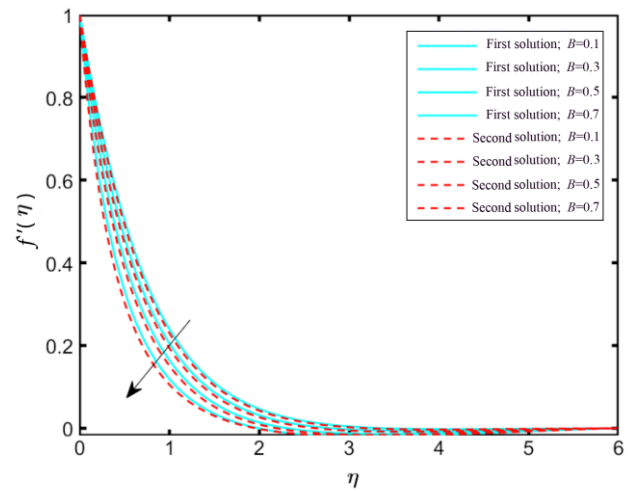


Figure 10. Influence of B on $f'(\eta)$.

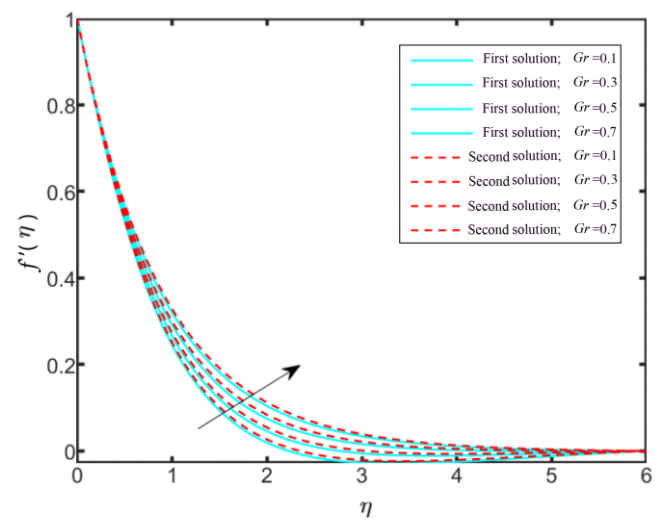


Figure 11. Influence of Gr on $f'(\eta)$.

thereby mitigating the resistance to stream and consequently leading to a decline in (S_f) . Figures 7–9 present a comprehensive analysis of the behavior of N_n and its dependence on the parameters Du , Ec , and Q for the HNF. Upon examining Figure 7, it is evident that as the value of the factor Du increases from 1 to 3, the heat transfer of HNF losses. Notably, it is crucial to highlight that the heat percentage experiences an enhancement in the second branch. This same pattern can be detected for the Ec factor's influence on N_n , as depicted in Figure 8. By analyzing the mathematical appearance of Ec , it becomes evident that Ec exhibits a straight relationship with velocity while an inverse relationship with heat transfer. Consequently, as the amount of Ec escalates, the fluidity intensifies, while the heat transfer rate decreases, resulting in a decrease in the value of N_n .

It is indeed intriguing to observe that the initial solution experiences a decline, whereas the subsequent solution undergoes an increment. Moreover, the mixed outline is practical for the second branch. In the range $0.2 < Pr < 0.7$, the Nusselt number surges, whereas in the range $0.7 < Pr < 0.8$, the heat transfer rate develops. Also, the Nusselt number decays when the level of Q (sink or source) are enhanced.

Figures 10–14 delve into the investigation of the fluctuation of the HNFs velocity profile $f'(\eta)$, taking into

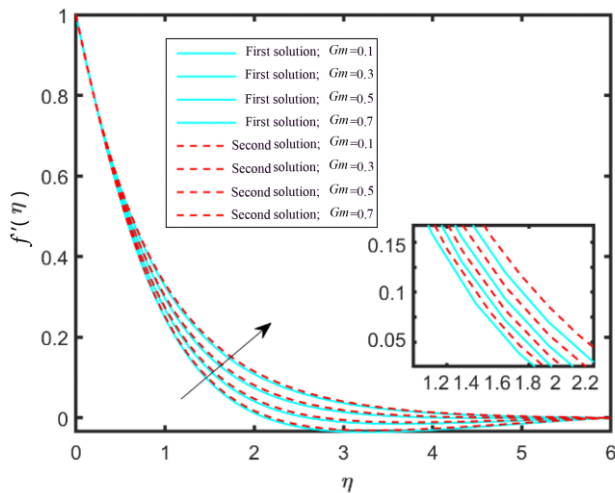


Figure 12. Influence of Gm on $f'(\eta)$.

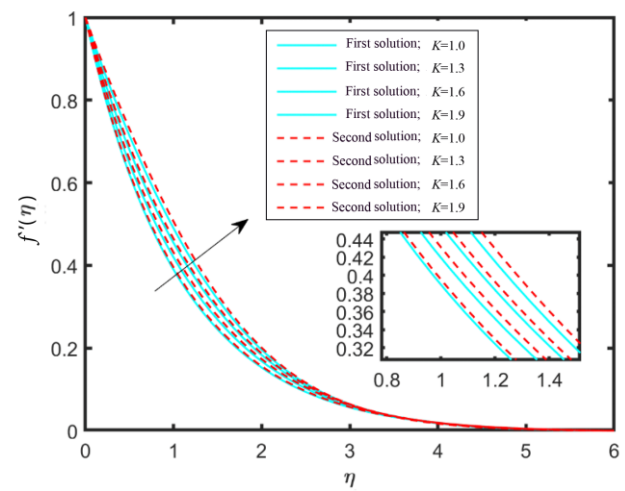


Figure 14. Influence of K on $f'(\eta)$.

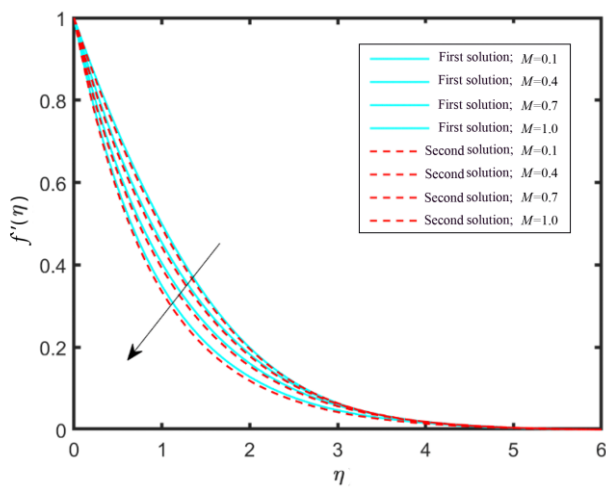


Figure 13. Influence of M on $f'(\eta)$.

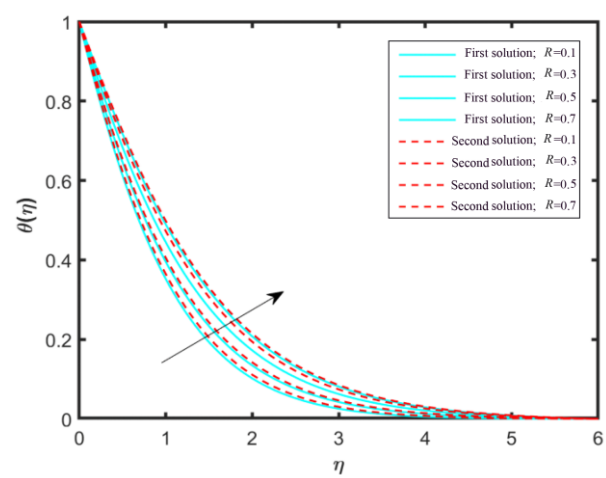
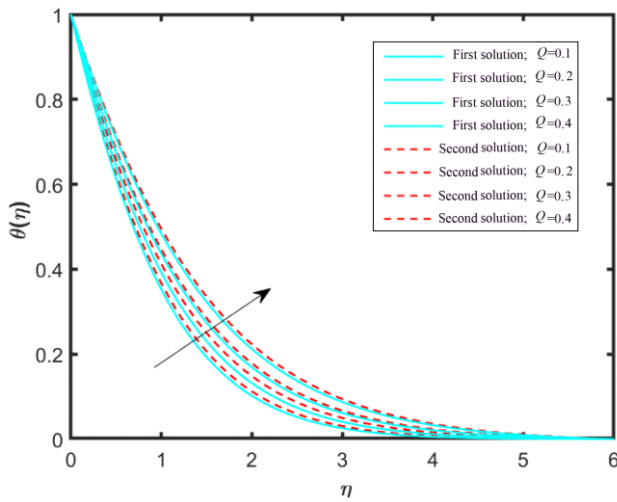
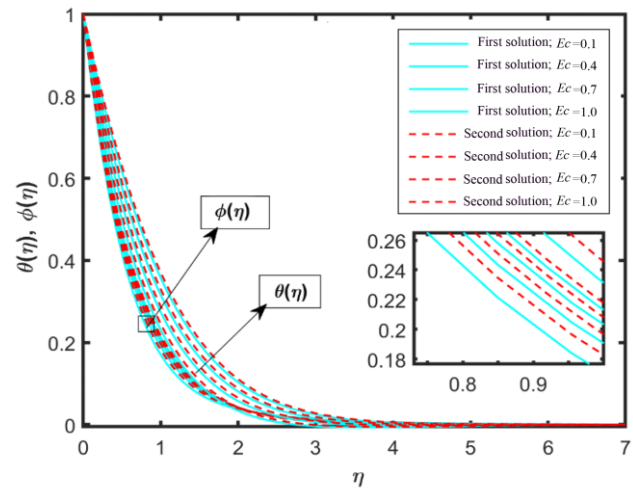
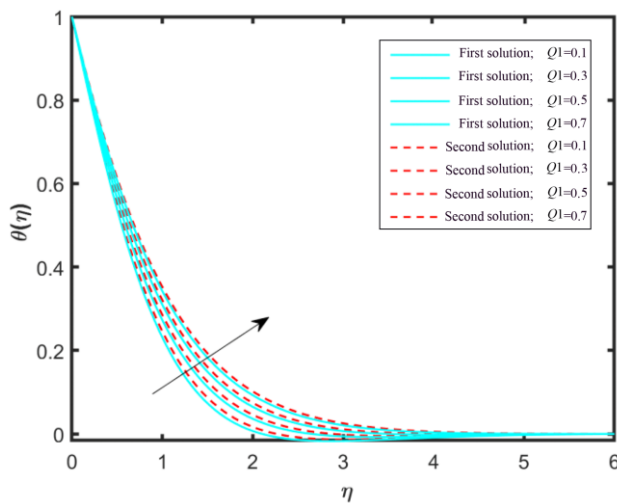
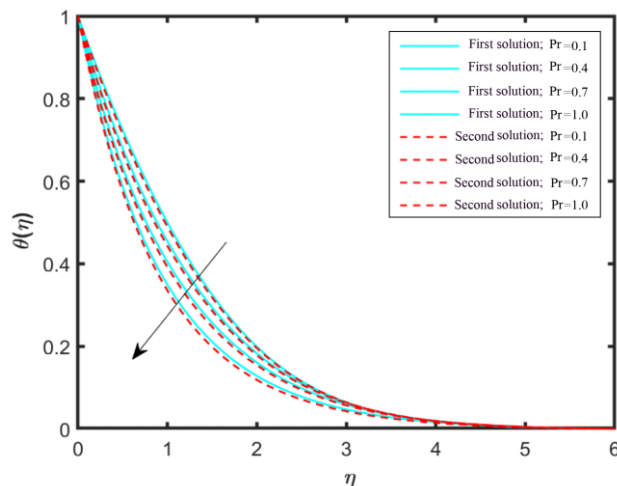


Figure 15. Influence of R on $\theta(\eta)$.

consideration various influential parameters such as B , Gr , Gm , M , and K . Figure 10 specifically focuses on the impact of B on fluid movement. Through a meticulous analysis of this figure, it has been observed that dual solutions have emerged as a result of the shrinking occurrences. It is crucial to note that the fluid motion experiences a decline as the amount of B is augmented. Moreover, it is intriguing to declaration at this juncture that the dominance of the first solution in comparison to the second solution is attributable to the intricate connection between the heat at the surface and the surrounding liquid. As the strengthening of B occurs, the aforementioned correlation becomes more significant, which in turn leads to a noticeable decrease in the value of $f'(\eta)$ within the specified range. Figures 11 and 12 delve into the examination of the correlation between the HNFs velocity and the Grashof number (Gr) and modified Grashof number (Gm). It is noteworthy to highlight that a similar influence is detected for both factors, meaning that the velocity of the HNFs experiences an escalation as the values of (Gr) and (Gm) increase. Taking into account both cases, it becomes evident that the velocity of the second branch surpasses than first. The Grashof number serves as a tool for comprehending the relationship between the dynamics of viscosity and the thermal buoyancy force, while the Gm serves as a means to identify the connection between the dynamics of viscosity and

the buoyancy force is related to the species being transferred. Thus, by increasing these factors, not only does the thermal buoyancy force rise but also the mass buoyancy force experiences an upsurge. Figures 13 and 14, on the other hand, aim to examine the variations of the M parameter and K factors on $f'(\eta)$. The investigation of diminishing performance is conducted for both velocities as the value of M , is enhanced. It is important to note that the profile $f'(\eta)$, which characterizes the fluid flow, displays a growing tendency with respect to the parameter K . As the level of M is augmented from 0.1 to 1, an interesting phenomenon occurs with the Lorentz force resulting from the presence of a magnetic field. This force acts as a hindrance to the motion of the fluid particles, leading to a deterioration in the fluid movement and a reduction in the depth of the boundary layer. This observation is depicted in Figure 14, where it is clearly demonstrated that the fluid motion intensifies as the values of the porosity factor increase within the range of 1 to 1.9. From a physical standpoint, the increase in the quantity of K causes the holes in the sheet to enlarge, thus facilitating a greater influx of fluid inside the sheet. Consequently, the motion of the fluid molecules becomes accelerated, resulting in a faster overall fluid motion.

Figures 15-18 delve into the examination of the effects of

Figure 16. Influence of Q on $\theta(\eta)$.Figure 19. Influence of Ec on $\theta(\eta)$ and $\phi(\eta)$.Figure 17. Influence of $Q1$ on $\theta(\eta)$.Figure 18. Influence of Pr on $\theta(\eta)$.

$R = Q = Q1$, and Pr on the temperature of HNFs. Figure 15 presents a graphical representation of the relationship between the temperature and the radiation factor R . Through this comprehensive analysis, it is elucidated that temperature exhibits a direct proportionality to R , meaning that when R increases, temperature also experiences an improvement in its value. This augmentation in temperature is accompanied

by an upsurge in the depth of the boundary layer. The rationale behind this phenomenon lies in the fact that as the radiation factor enhances from 0.1 to 0.7, more heat is transmitted to the HNFs, leading to an upsurge in its temperature. Furthermore, the thermal diffusion process is significantly enhanced as a result of the larger quantities of R present, which in turn governs the enhancement of the fluid temperature of the HNFs. It is important to note that this increasing trend is observed for both solutions. Upon analyzing Figures 16 and 17, it is discerned that temperature experiences a growth pattern in relation to Q and $Q1$, respectively, within the range of 0.1 to 0.7. This physical occurrence can be ascribed to the absorption (generation) of heat, which happens in the warm area, as the values of Q and $Q1$ persistently increase. The occurrence of an unusually high quantity of intensity within the liquid serves to stimulate the enhancement of atomic power within the HNF. This, in turn, leads to the upsurge of the Boundary Layer Thickness (BLT) and consequently facilitates the transport of heat energy, thereby significantly improving the temperature of the system. In order to investigate the effect of the Prandtl number (Pr) on heat of the HNFs, a schematic representation, denoted as Figure 18, has been devised. The phenomenon of thermal radiation can be understood as the ratio between the thermal diffusivity and the momentum diffusivity. With an upsurge in Pr , there is an accompanying decrease in both the thermal diffusivity and the heat dissipation, albeit to a slight extent. As a result, the heat rate experiences a minor enhancement, leading to a rapid decline in heat of the HNFs, as exemplified in Figure 18.

Figures 19-21 visually depict the influence of Ec , Du , and Sr on the distribution of temperature and concentration. In the case of Ec , Figure 19 delves into the relationship between Ec and the profiles of temperature and concentration. This analysis reveals the existence of dual solutions for both temperature and concentration when Ec serves as the driving force. It is noteworthy that an increasing trend is observed in both profiles as the Ec values are augmented from 0.1 to 1. It is intriguing to observe that the variation in the second solution surpasses that of the first. From a physical standpoint, when the magnitude of Ec is heightened, the mechanical energy experiences a rapid transformation into thermal energy, thereby

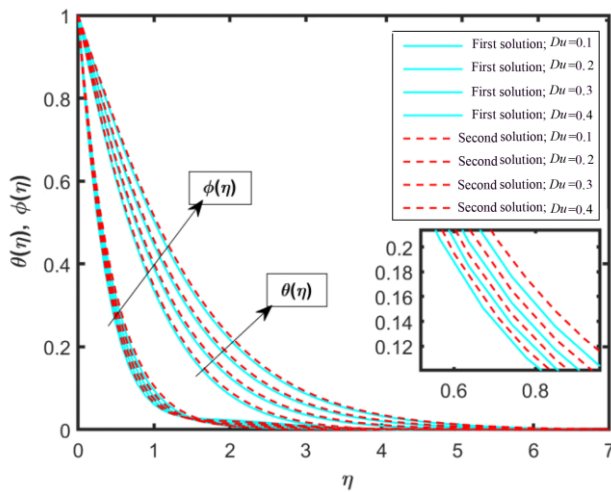


Figure 20. Influence of Du on $\theta(\eta)$ and $\phi(\eta)$.

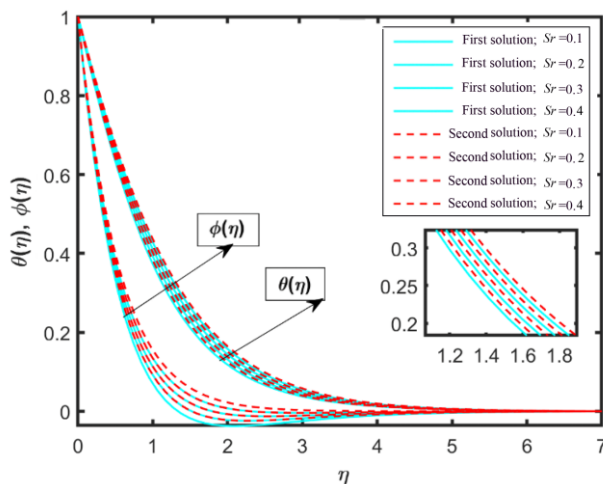


Figure 21. Influence of Sr on $\theta(\eta)$ and $\phi(\eta)$.

remarkably enhancing the temperature of the HNFs throughout the entire channel. The growth of indicates a rise in the conversion of mechanical energy into thermal energy, resulting in an overall elevation in temperature. Correspondingly, the influence of Du on the fluctuations of temperature and concentration is depicted in Figure 20. The performance exhibited by Du regarding temperature and concentration is shown as deliberated in Figure 19 for Ec . The disparity in temperature is found to be more noteworthy than concentration. The temperature increase is directly correlated to the intensity of Du because of its influence on the thermal slopes of concentration inside the liquid. Hence, a higher amount of Du results in an augmentation of temperature and the depth of the thermal BL. Figure 21 delves into the examination of the impact of Sr on the fluctuations in temperature and concentration. This all-encompassing examination demonstrates that the augmentation in Sr leads to a simultaneous increase in both temperature and concentration. It is evident that as the magnitude of Sr elevates from 0.1 to 0.4, there is a notable escalation in HNFs temperature as well as concentration. Furthermore, it is wealth mentioning that the rise in heat is deemed to be more significant in comparison to concentration for both branches of solutions. This can be attributed to the emergence of a substantial mass diffusivity

phenomenon, which is only manifested when Sr is heightened from 0.1 to 0.4.

6. Conclusion

The main aim of the current investigation is to scrutinize the phenomenon of cross-diffusion of magnetized Hybrid Nanofluid (HNF) above an elongated or contracting surface in the presence of thermal conductivity. In order to assess the stability of the scheme, the eigenvalues are computed. It is noteworthy that the existence of the smallest positive eigenvalues signifies the presence of stable solutions, whereas the negative eigenvalues indicate the existence of unstable solutions. The mathematical representation of the flow models is transformed into ODEs via resemblance transformations. The statistical outcomes are achieved by employing the BVP4C technique. To provide a comprehensive understanding of the physical factors governing fluid dynamics, the graphical and tabular representations are utilized to elaborate upon the inspiration behind these factors. This finding was reported by Dero et al. [30] and has since been supported by numerous studies in the field. The importance of conducting a stability analysis cannot be overstated, as it allows researchers to understand the behavior of a system when duality arises.

1. In particular, dual variation is often witnessed for the factors B and M on S_f . This dual fluctuation phenomenon is characterized by an increase in S_f in the first branch and a subsequent decrease in S_f in the second branch.
2. Moreover, it has been observed that as the amount of M increases from 1 to 3, S_f also increases. Also, when the parameter B is increased from 1 to 5, S_f exhibits a corresponding rise. These findings suggest a positive relationship between M , B and S_f . However, it is important to note that the relationship between S_f and other variables, such as Gr and M is more complex.
3. In fact, it has been investigated that S_f tends to decrease as the quantities of Gr and M are increased for both of the HNF models. This finding highlights the intricate interplay between various parameters and their impact on the stability of the system.
4. It is widely acknowledged that as the magnitude of Du increases from 1 to 3, there is a discernible reduction in the heat transfer rate in HNFs. In the context of fluid dynamics, it has been determined that the fluid velocity experiences a decline when the values of variable B are increased.
5. By analyzing the behavior of the velocity branches, it becomes evident that both branches exhibit a decreasing trend as the M is improved. On the other hand, the velocity profile displays a growing trend with respect to variable K . This increasing trend suggests that the variation in velocity is positively influenced by the values of variable K varying from 1 to 1.9.
6. Furthermore, a comprehensive analysis of the temperature variable reveals that it is directly proportional to the variable R . This direct

proportionality suggests that as the variable R increases, the temperature also increases.

7. Additionally, it has been reported that the temperature is a growing function of variables Q and QI , with values ranging from 0.1 to 0.7. This growing function implies that as the values of Q and QI increase within the specified range, the temperature also exhibits an upward trend.
8. Similarly, an increasing phenomenon has been reported for the temperature and concentration profiles as the amounts of variable Ec are improved from 0.1 to 1.

Theoretical analysis's conclusions have important ramifications for many industries, comprising technology, automobile solar thermal and cooling systems, lubricating properties, hybrid power plants, metallic welding procedures, and healthcare product manufacturing. These applications underscore the results' practical value and their potential influence on a wide range of sectors.

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Authors contribution statement

First author: Conceptualization; Methodology; Formal analysis; Investigation; Data curation; Software; Validation; Visualization; Writing—original draft; Writing—review and editing.

Second author: Conceptualization; Methodology; Formal analysis; Software; Validation; Visualization; Supervision; Writing—review and editing.

Third author: Investigation; Data curation; Formal analysis; Validation; Resources; Writing—review and editing.

Fourth author: Methodology; Software; Data analysis; Visualization; Validation; Writing—review and editing.

Fifth author: Conceptualization; Supervision; Project administration; Resources; Validation; Writing—review and editing.

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