



# Thermal applications of hybrid nanofluid containing carbon nanotubes with heat source and radiative effects

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Ethylene Glycol (EG);  
Rotating disk;  
Slip effects.

## Abstract

The objective of the current work is to characterize the thermal impact of Carbon Nanotubes (CNTs) due to a rotating disk, with applications of thermal radiation, heat source, and slip effects. Single-Walled Carbon Nano-Tubes (SWCNTs) and Multi-Walled Carbon Nano-Tubes (MWCNTs) with a suspension of Ethylene Glycol (EG) have been used to analyze the problem. The base fluid consequences are justified by using the Casson fluid. The flow model is justified by the interaction of velocity and thermal slip effects. Thermal characteristics of SWCNT and MWCNT along EG base materials have been presented. The heat transfer investigation is based on the implementation of the Cattaneo-Christov approach. Numerical computations are performed with the help of the shooting scheme. Comparative thermal analysis is performed for traditional nanofluid (SWCNT/EG) and hybrid nanofluid (SWCNTs-MWCNTs/EG). Physical visualization of results for the enhancement of the heat transfer phenomenon is performed. It has been observed that the heat transfer phenomenon is more pronounced for the hybrid nanofluid (SWCNTs-MWCNTs/EG) as compared to the nanofluid (SWCNT/EG). The thermal profile improves for the Casson fluid parameter.

## 1. Introduction

Hybrid nanomaterials are a modified class of nanofluids having efficient thermal properties. The hybrid nanofluid represents the joint suspension of two distinct nanoparticles with a base fluid. The interaction of two different nanoparticles shows stronger thermal performance as compared to common nanofluids. Owing to high thermal impact, the hybrid nanofluids offer various kinds of applications in refrigeration, nuclear systems, heat exchangers, chemical reactions, aircraft, thermal reservoirs, etc. Researchers have performed various investigations for studying the hybrid nanofluid thermal impact. For instance, Sundar et al. [1] focused on investigating the thermal interpretation of hybrid nanofluid under the influence of different

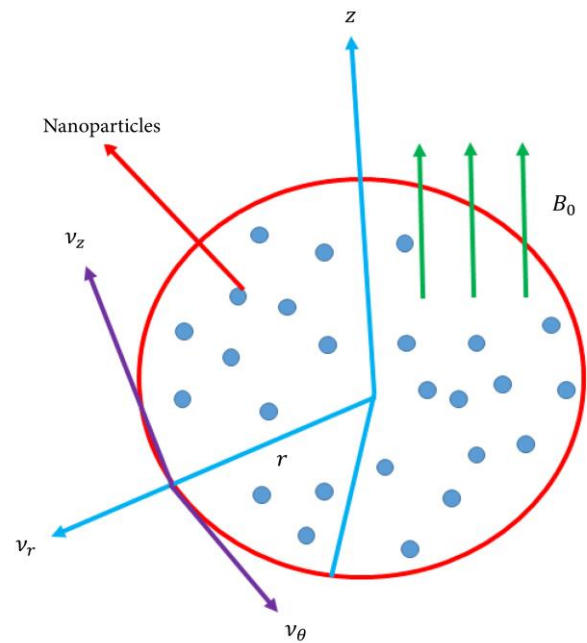
friction sources. Ahmad et al. [2] addressed the heat transfer impact due to graphene oxide and silver nanoparticles in order to evaluate the boosted performance of kerosene oil-based liquid. Ali et al. [3] predicted the thermo-fluid aspects of a hybrid nanofluid due to a Couette channel. Faridi et al. [4] predicted the heat fluctuation of a hybrid nanofluid due to stretched surface flow. Analysis highlighting the thermal reservations of Carbon Nanotubes (CNTs) confined to a curved surface was elaborated by Abideen and Saif [5]. Mebarek-Oudina et al. [6] visualized the hydromagnetic flow of magnetite nanoparticles to improve the heat transfer phenomenon. Borode et al. [7] worked out artificial neural network analysis for describing the thermophysical

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properties of hybrid nanofluid via an experimental approach. Manjakuppam and Sonawane [8] deduced the thermal simulations based on hybrid nanofluid flow with significance to heat exchangers. Titanium oxide and silica nanoparticles were used to improve the thermal performance of water-based fluid. Alawi et al. [9] described solar collector applications due to the utilization of hybrid nanomaterials. The results were supported by machine learning algorithms. The squeezing flow of copper oxide and aluminum nanoparticles for Darcy-Forchheimer applications has been analyzed by Hayat et al. [10]. Acharya and Öztöp [11] present an investigation of energy storage due to the semi-circular flow of hybrid nanofluid. Srilatha et al. [12] studied the machine learning analysis for the interface layer of hybrid nanofluid due to a porous disk. Foukhari et al. [13] performed an evaluation of entropy production due to a hybrid nanofluid due to two coaxial porous cylinders. Sarfaraz and Khan [14] claimed the heat transfer improvement with the interaction of a hybrid nanofluid in a wedge-shaped surface. Mehdi et al. [15] utilized the entropy generation effects in curved surface flow comprising the hybrid nanofluid. Rostami et al. [16] studied the thermal outcomes for dust particles with a mixture of hybrid nanofluid. Zangoee et al. [17] used the interference of slip to inspect the diverse thermal mechanisms of hybrid nanofluid. Hosseinzadeh et al. [18] performed the heat transfer computations based on iron oxide and molybdenum disulfide nanoparticles in a sinusoidal cylinder. Comparative thermal observations for the thermal evaluation associated with concave parabolic, trapezoidal, and convex cross configurations with utilization of hybrid nanofluid have been inspected by Hosseinzadeh et al. [19]. Paul et al. [20] depicted the contribution of a Casson hybrid nanofluid governed by an exponentially stretched cylinder. An investigation for improvement of heat fluctuation in vertically driven flow of hybrid nanofluid was proposed by Paul et al. [21]. Sarma and Paul [22] analyzed the bioconvective achievement for decomposition of hybrid nanoparticles. Copper oxide and gold nanoparticles were used to investigate the thermal phenomenon. The heat fluctuation due to ternary hybrid nanofluid in a rotating disk was visualized by Paul et al. [23]. In another investigation, Paul et al. [24] utilized the Hall effect in Casson hybrid nanofluid flow with fluctuation of heat transfer.

In the above-cited research work, it has been noticed that various studies have been performed to analyze the heat transfer due to hybrid nanofluid. However, comparative thermal observations for nanofluid and hybrid nanomaterial due to a rotating disk with slip effects have not been focused on yet. Therefore, the objective of the current work is to study comparative thermal analysis due to radiative flow of hybrid nanofluid with the application of slip effects and an external



**Figure 1.** Illustration of the flow problem.

heat source. The hybrid nanofluid is based on the interaction of Single Walled Carbon Nano-Tubes (SWCNTs) and Multi-Walled Carbon Nano-Tubes (MWCNTs) with Ethylene Glycol (EG) base fluid. Comparative thermal simulations are presented for traditional nanofluid (SWCNTs/EG) and hybrid nanofluids (SWCNTs-MWCNTs/EG). The novel aspects of this investigation are:

- A suspension of SWCNTs and MWCNTs with EG due to a rotating disk has been considered;
- The base fluid properties are highlighted by the Casson fluid model;
- The investigation is subject to velocity and thermal slip constraints;
- The heat transfer model is updated with the implementation of Cattaneo-Christov theory;
- Numerical computations associated with the flow problem are performed with a shooting scheme;
- Comparative analysis is performed for prediction of heat transfer for traditional nanofluid (SWCNTs/EG) and hybrid nanofluids (SWCNTs-MWCNTs/EG).

## 2. Formulation of the problem

Let us observe the heat transfer analysis due to the interaction of SWCNTs and MWCNTs with the EG base liquid. The flow problem is modeled in view of the following flow assumptions:

- Assuming a steady flow transport of Ethylene Glycol base fluid with a suspension of SWCNTs and MWCNTs.
- The rotatory disk accounts for the flow as shown in Figure 1.

- For development of mathematical model, the cylindrical coordinates are used with coordinates  $r, \theta$  and  $z$ . Denoting velocity components with  $v_r, v_\theta$  and  $v_z$ .
- The rotation of the disk is considered along the  $z$ -direction maintain angular velocity  $\Omega$ .
- Slip effects for both temperature and velocity profiles have been considered [25].
- The heat source and radiation significance for the inspection of heat transfer are considered.
- The upgraded energy equation is used with the implication of the modified Fourier law.

The governing equations for the stated flow constraints are expressed as [5,25].

$$\frac{\partial v_r}{\partial r} + \frac{v_r}{r} + \frac{\partial v_z}{\partial z} = 0, \quad (1)$$

$$\rho_{hnf} \left( v_r \frac{\partial v_r}{\partial r} + v_z \frac{\partial v_r}{\partial z} - \frac{v_\theta^2}{r} \right) = \mu_{hnf} \left( 1 + \frac{1}{\gamma} \right) \left( \frac{\partial^2 v_r}{\partial r^2} + \frac{1}{r} \frac{\partial v_r}{\partial r} + \frac{\partial^2 v_r}{\partial z^2} - \frac{v_r}{r^2} \right) - \sigma_{hnf} B_0^2 v_r, \quad (2)$$

$$\rho_{hnf} \left( v_r \frac{\partial v_\theta}{\partial r} + v_z \frac{\partial v_\theta}{\partial z} - \frac{v_r v_\theta}{r} \right) = \mu_{hnf} \left( 1 + \frac{1}{\gamma} \right) \left( \frac{\partial^2 v_\theta}{\partial r^2} + \frac{1}{r} \frac{\partial v_\theta}{\partial r} + \frac{\partial^2 v_\theta}{\partial z^2} - \frac{v_\theta}{r^2} \right) - \sigma_{hnf} B_0^2 v_\theta, \quad (3)$$

$$\rho_{hnf} \left( v_r \frac{\partial v_z}{\partial r} + v_z \frac{\partial v_z}{\partial z} \right) = \mu_{hnf} \left( 1 + \frac{1}{\gamma} \right) \left( \frac{\partial^2 v_z}{\partial r^2} + \frac{1}{r} \frac{\partial v_z}{\partial r} + \frac{\partial^2 v_z}{\partial z^2} \right), \quad (4)$$

with boundary conditions [2]; We have Eq. (5) is shown in Box I.

$$v_r = rs + L_0 \left( 1 + \frac{1}{\gamma} \right) \frac{\partial v_r}{\partial z}, \quad v_\theta = r\Omega + L_0 \left( 1 + \frac{1}{\gamma} \right) \frac{\partial v_\theta}{\partial z},$$

$$v_z = 0, T = T_w + N_0 \frac{\partial T}{\partial z}, \quad \text{at } z = 0. \quad (6)$$

$$v_r \rightarrow 0, \quad v_\theta \rightarrow 0, \quad T \rightarrow T_\infty \quad \text{as } z \rightarrow \infty. \quad (7)$$

With  $\mu_{hnf}$  (dynamic viscosity of hybrid nanoparticles),  $T_w$  (surface temperature),  $\gamma$  (Casson fluid coefficient),  $B_0$  (magnetic field strength),  $(\rho C_p)_{hnf}$  (heat capacitance),  $T$  (fluid temperature),  $L_0$  (velocity slip coefficient),  $N_0$  (thermal slip coefficient),  $\rho_{hnf}$  (hybrid nanofluid density),  $\lambda_t$  (thermal

**Table 1.** Thermal properties SWCNTs and MWCNTs with EG base liquid.

| Physical properties     | Ethylene Glycol (WE) | SWCNT           | MWCNT                |
|-------------------------|----------------------|-----------------|----------------------|
| Density                 | 1059.68              | 2600            | 1600                 |
| Specific heat           | 335257               | 425             | 796                  |
| Thermal conductivity    | 0.404                | 6600            | 3000                 |
| Electrical conductivity | 0.00276              | $10^6$ - $10^7$ | $1.9 \times 10^{-4}$ |

relaxation time),  $\sigma^*$  (Stefan Boltzmann constant),  $T_\infty$  (free stream temperature),  $\alpha_{hnf}$  (thermal diffusivity),  $Q_0$  (external heat source coefficient), and  $k^*$  (absorption coefficient). Numerical values for various thermal properties of SWCNTs-MWCNTs/EG suspension have been expressed in Table 1.

To transform the problem into dimensionless form, the following similarity transformations are suggested [5,25]:

$$v_r = r\Omega f'(\zeta), \quad v_\theta = r\Omega h(\zeta), \quad v_z = -(2\Omega\nu_f)^{1/2} f(\zeta),$$

$$\theta(\zeta) = \frac{T - T_\infty}{T_w - T_\infty}, \quad \zeta = z \left( \frac{2\Omega}{\nu_f} \right)^{1/2}. \quad (8)$$

The dimensionless form is:

$$2 \left( 1 + \frac{1}{\gamma} \right) f''' - \zeta_1 [f'^2 - 2ff'' - h^2 + \zeta_2 Mf'] = 0, \quad (9)$$

$$2 \left( 1 + \frac{1}{\gamma} \right) h'' + \zeta_1 [2fh' - 2fh - \zeta_3 Mh] = 0, \quad (10)$$

$$(\zeta_4 + Rd)\theta'' + Pr Q\theta + \zeta_2 Pr [f\theta' - \alpha(f^2\theta'' + ff'\theta')] = 0, \quad (11)$$

and the boundary conditions are given below:

$$f(0) = 0, \quad f'(0) = A + \left( 1 + \frac{1}{\gamma} \right) \delta f''(0),$$

$$h(0) = 1 + \left( 1 + \frac{1}{\gamma} \right) \delta f'(0), \quad (12)$$

$$\theta(0) = 1 + \beta\theta'(0), \quad f'(\infty) = h(\infty) = \theta(\infty) \rightarrow 0. \quad (13)$$

where  $M$  (Hartmann constant),  $Pr$  (Prandtl constant),  $\alpha$  (thermal relaxation coefficient),  $A$  (stretching constant),  $\delta$  (velocity slip parameter) and  $\beta$  (thermal slip parameter),  $Rd$  (thermal radiation) and  $Q$  (heat generation) which are defined

$$v_r \frac{\partial T}{\partial r} + v_z \frac{\partial T}{\partial z} = \alpha_{hnf} \left( \frac{\partial^2 T}{\partial r^2} + \frac{1}{r} \frac{\partial T}{\partial r} + \frac{\partial^2 T}{\partial z^2} \right) - \frac{16}{3} \frac{\sigma^* T_\infty^3}{k^* (\rho C_p)_{hnf}} \left( \frac{\partial^2 T}{\partial r^2} + \frac{1}{r} \frac{\partial T}{\partial r} + \frac{\partial^2 T}{\partial z^2} \right)$$

$$- \lambda_t \left[ v_r^2 \frac{\partial^2 T}{\partial r^2} + v_z^2 \frac{\partial^2 T}{\partial z^2} + 2v_r v_z \frac{\partial^2 T}{\partial r \partial z} + \left( v_r \frac{\partial v_r}{\partial r} + v_z \frac{\partial v_r}{\partial z} \right) \frac{\partial T}{\partial r} + \left( v_r \frac{\partial v_z}{\partial r} + v_z \frac{\partial v_z}{\partial z} \right) \frac{\partial T}{\partial z} \right] - \frac{Q_0}{(\rho C_p)_{hnf}} (T - T_\infty), \quad (5)$$

Box I

**Table 2.** Thermo-physical features of nanofluid (SWCNTs/EG) and hybrid nanofluids (SWCNTs-MWCNTs/WE) [5].

| Properties              | Hybrid nanofluid<br>(SWCNT-MWCNT/WE)                                                                                                                                                                                                                                                                                                                                                 | Nanofluid<br>(SWCNT/WE)                                                                                                             |
|-------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------|
| Electrical conductivity | $\frac{\sigma_{hnf}}{\sigma_f} = \frac{\sigma_{SWCNT} - 2\phi_{SWCNT}(\sigma_{nf} - \sigma_{SWCNT}) + 2\sigma_{nf}}{\sigma_{SWCNT} + \phi_{SWCNT}(\sigma_{nf} - \sigma_{SWCNT}) + 2\sigma_{nf}}$ $\frac{\sigma_{nf}}{\sigma_f} = \frac{\sigma_{MWCNT} - 2\phi_{SWCNT}(\sigma_f - \sigma_{MWCNT}) + 2\sigma_f}{\sigma_{MWCNT} + \phi_{MWCNT}(\sigma_f - \sigma_{MWCNT}) + 2\sigma_f}$ | $\frac{\sigma_{nf}}{\sigma_f} = 1 + \frac{3(\sigma - 1)\phi}{(\sigma + 2) - (\sigma - 1)\phi}$ $\frac{\sigma_s}{\sigma_f} = \sigma$ |
| Viscosity               | $\mu_{hnf} = \frac{\mu_f}{(1 - \phi_{SWCNT})^{2.5} (1 - \phi_{MWCNT})^{2.5}}$                                                                                                                                                                                                                                                                                                        | $\mu_{nf} = \frac{\mu_f}{(1 - \phi)^{2.5}}$                                                                                         |
| Heat capacity           | $(\rho C_p)_{hnf} = (\rho C_p)_f (1 - \phi_{SWCNT})$ $\left[ (1 - \phi_{MWCNT}) \left( \rho C_p \right)_{MWCNT} + \phi_{MWCNT} \left( \rho C_p \right)_f \right] + \phi_{SWCNT} (\rho C_p)_{SWCNTs}$                                                                                                                                                                                 | $(\rho C_p)_{nf} = (\rho C_p)_f (1 - \phi) + \phi \left( \frac{(\rho C_p)_s}{(\rho C_p)_f} \right)$                                 |
| Density                 | $\rho_{hnf} = \rho_{SWCNT} \phi_{SWCNT} + \left[ (1 - \phi_{SWCNT}) \left\{ (1 - \rho_{MWCNT}) \rho_f \right\} + \rho_{MWCNT} \phi_{MWCNT} \right]$                                                                                                                                                                                                                                  | $\rho_{nf} = \rho_s \phi + (1 - \phi) \rho_f$                                                                                       |
| Thermal conductivity    | $\frac{k_{hnf}}{k_f} = \frac{(k_{SWCNT} + (n-1)k_{nf}) - (n-1)\phi_{SWCNT}(k_{nf} - k_{SWCNT})}{(k_{SWCNT} + (n-1)k_{hnf}) + \phi_{SWCNT}(k_{nf} - k_{SWCNT})}$                                                                                                                                                                                                                      | $\frac{k_{nf}}{k_f} = \frac{(k_s + (n-1)k_f) - \phi(k_f - k_s)}{(k_s + (n-1)k_f) + \phi(k_f - k_s)}$                                |

$$\text{as: } M = \sigma_f \frac{B_0^2}{\rho_f} \Omega, \quad \text{Pr} = \frac{\nu_f}{\alpha_f}, \quad \alpha = 2\lambda_t \Omega, \quad \times \left[ \frac{(k_{s1} + 2k_f) - 2\phi_2(k_f - k_{s1})}{(k_{s1} + 2k_f) + \phi_2(k_f - k_{s1})} \right]. \quad (17)$$

$$A = \frac{s}{\Omega}, \quad \delta = L_0 \left( \frac{2\Omega}{\nu_f} \right)^{1/2}, \quad \beta = N_0 \left( \frac{2\Omega}{\nu_f} \right)^{1/2},$$

$$Rd = \frac{4 \sigma^* T_\infty^3}{3 k^* k_f}, \quad Q = \frac{Q_0}{(\rho C_p)_{hnf}}.$$

Thermo-physical constants involved in the transformed equations are defined as:

$$\zeta_1 = (1 - \phi_1)^{2.5} (1 - \phi_2)^{2.5} \left[ (1 - \phi_2) \left\{ (1 - \phi_1) + \phi_1 \frac{\rho_{s1}}{\rho_f} \right\} + \phi_2 \frac{\rho_{s2}}{\rho_f} \right], \quad (14)$$

$$\zeta_2 = (1 - \phi_1)^{2.5} (1 - \phi_2)^{2.5} \frac{\sigma_{hnf}}{\sigma_f}, \quad (15)$$

$$\zeta_3 = \left[ (1 - \phi_2) \left\{ (1 - \phi_1) + \phi_1 \frac{(\rho C_p)_{s1}}{(\rho C_p)_f} \right\} + \phi_2 \frac{(\rho C_p)_{s2}}{(\rho C_p)_f} \right], \quad (16)$$

$$\zeta_4 = \frac{k_{hnf}}{k_f} = \left[ \frac{(k_{s2} + 2k_{nf}) - 2\phi_1(k_{nf} - 2k_{s2})}{(k_{s2} + 2k_{nf}) + \phi_1(k_{nf} - 2k_{s2})} \right]$$

Where  $\phi_1$  defines the solid volume fractions of SWCNTs while  $\phi_2$  be the volume fractions of MWCNTs. The mathematical expressions for hybrid nanofluid (SWCNTs-MWCNTs/EG) and nanofluid (SWCNTs/EG) are presented in Table 2.

Physical quantities skin friction and Nusselt number are defined by:

$$C_f = \frac{\tau_w}{\rho(\Omega r)^2}, \quad \tau_w = \mu_{hnf} \left( \frac{\partial u}{\partial y} \right)_{z=0},$$

$$Nu_x = \frac{r q_w}{k_f (T_w - T_\infty)}, \quad q_w = -k_{hnf} \left( \frac{\partial T}{\partial r} \right)_{z=0}, \quad (18)$$

$$(\text{Re}_r)^{1/2} C_f = \frac{\left( 1 + \frac{1}{r} \right)}{(1 - \phi_1)^{2.5} (1 - \phi_2)^{2.5}} f''(0), \quad (19)$$

$$(\text{Re}_r)^{-1/2} Nu_r = - \left( \frac{k_{hnf}}{k_f} \right) \theta'(0). \quad (20)$$

Where  $\text{Re}_r = \frac{(\Omega r) r}{\nu_f}$  is the local Reynolds number.

**Table 3.** Comparison of numerical results with the study of Mustafa [26] taking  $A=0$ ,  $\phi_1 = \phi_2 = 1$  and  $\gamma \rightarrow \infty$ .

| Parameters |          | Mustafa [26] |          | Present results |          |
|------------|----------|--------------|----------|-----------------|----------|
| $M$        | $\delta$ | $f'(0)$      | $f''(0)$ | $f'(0)$         | $f''(0)$ |
| 0.0        | 0.25     | 0.064883     | 0.259534 | 0.064885        | 0.259535 |
| 0.2        | 0.25     | 0.047794     | 0.191176 | 0.047795        | 0.191177 |
| 0.4        | 0.25     | 0.036514     | 0.146057 | 0.036513        | 0.146056 |

### 3. Numerical computations

This section incorporates the implementation of the shooting scheme for a set of modeled equations. To initiate the simulations, the higher-order system is first converted into a first-order system with the help of following transformations:

$$(s_1, s_2, s_3, s_4, s_5, s_6, s_7) = (f, f', f'', h, h', \theta, \theta'), \quad (21)$$

$$\begin{pmatrix} s_1' \\ s_2' \\ s_3' \\ s_4' \\ s_5' \\ s_6' \\ s_7' \end{pmatrix} = \begin{pmatrix} s_2 \\ s \\ \frac{\zeta_1(s_2^2 - 2s_1s_3 - s_4^2 + \zeta_2Ms_2)}{2\left(1 + \frac{1}{r}\right)} \\ s_5 \\ \frac{-\zeta_1}{2\left(1 + \frac{1}{r}\right)}[2s_1s_5 - 2s_2s_4 - \zeta_2Ms_4] \\ s_7 \\ \frac{1}{((\zeta_4 + Rd) - \text{Pr}\alpha s_1^2)}[\zeta_3 \text{Pr} s_1 s_7 (\alpha s_2 - 1) - \text{Pr} Q s_6] \end{pmatrix} \quad (22)$$

The boundary conditions are reduced to:

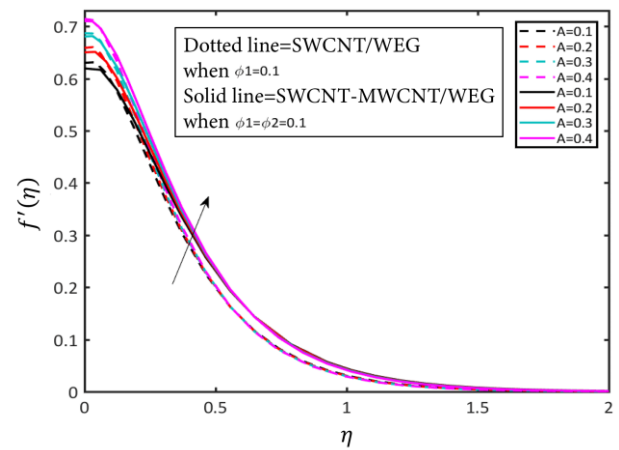
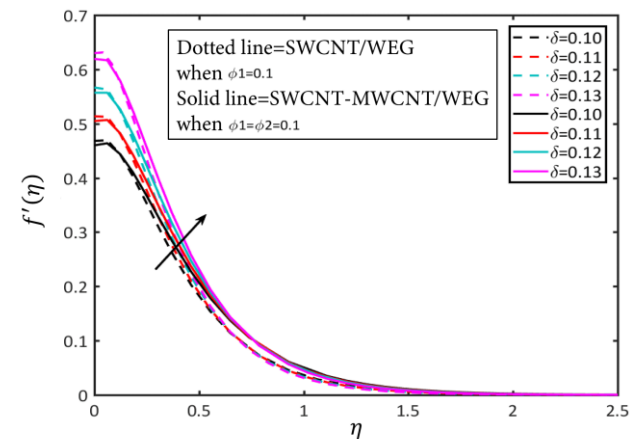
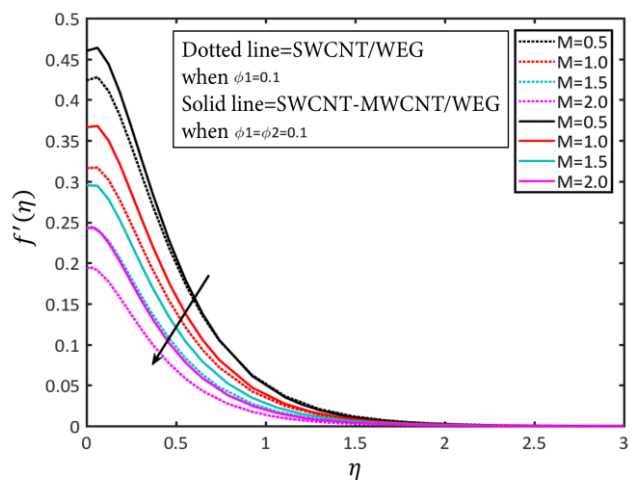
$$\begin{pmatrix} s_1(0) \\ s_2(0) \\ s_3(0) \\ s_4(0) \\ s_5(0) \\ s_6(0) \\ s_7(0) \end{pmatrix} = \begin{pmatrix} 0 \\ A + \left(1 + \frac{1}{r}\right)\delta s_1 \\ s_1 \\ 1 + \left(1 + \frac{1}{r}\right)\delta s_2(0) \\ s_2 \\ 1 + \beta s_3 \\ s_4 \end{pmatrix}. \quad (23)$$

### 4. Validation of results

The simulated numerical data have been confirmed by comparison with the investigation of Mustafa [26]. Table 3 shows that the current numerical results claim fine accuracy compared with Mustafa [26].

### 5. Results and discussion

Physical interpretation of results has been visualized in this section. Comparative results are prepared for both nanofluid (SWCNTs/EG) and hybrid nanofluids (SWCNTs MWCNTs/EG) with variation of modeled parameters. Figure 2 interprets the contribution of stretching constant  $A$  on radial velocity  $f'$ .

**Figure 2.** Velocity profile  $f'$  for  $A$ .**Figure 3.** Velocity profile  $f'$  for  $\delta$ .**Figure 4.** Velocity profile  $f'$  for  $M$ .

arising numeric values, the radial velocity increases for both fluids. The enhancement in  $f'$  is more prominent for SWCNTs-MWCNTs/EG decomposition. Figure 3 helps to visualize the significance of the velocity slip parameter  $\delta$  on  $f'$  for both SWCNTs/EG and SWCNTs-MWCNTs/EG suspensions. Leading values of  $\delta$  slow down the velocity for both decompositions. The momentum boundary layer also becomes thinner with increasing variation of  $\delta$ . The physical description discussed in Figure 4 shows the truncated profile of  $f'$  upon increasing Hartmann number  $M$ .

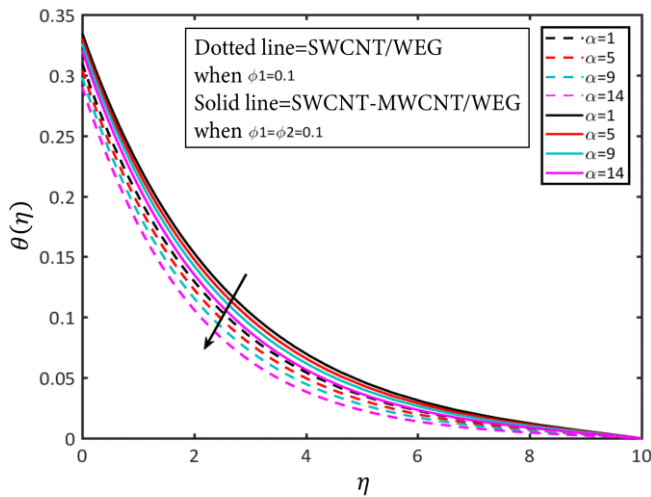


Figure 5. Temperature profile  $\theta$  for  $\alpha$ .

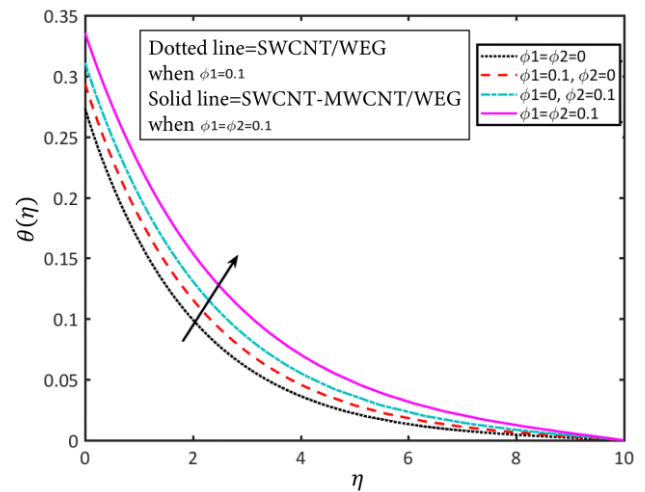


Figure 7. Temperature profile  $\theta$  for Casson fluid, Casson nanofluid and Casson hybrid nanofluid.

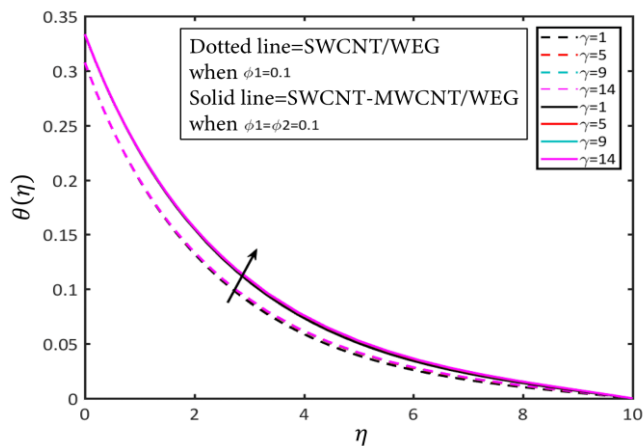


Figure 6. Temperature profile  $\theta$  for  $\gamma$ .

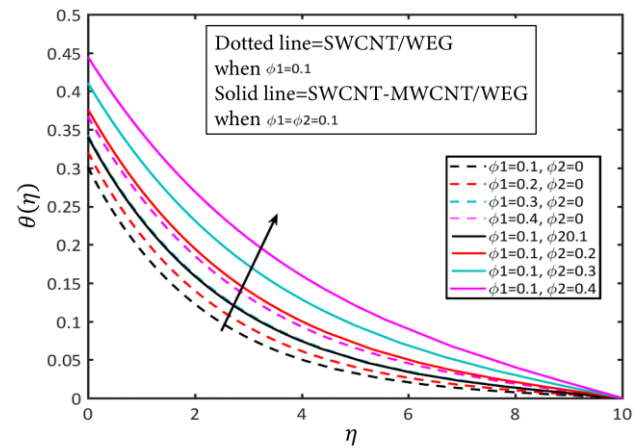


Figure 8. Temperature profile  $\theta$  for  $\phi_1=0.1$ ,  $\phi_2=0$

The velocity profile gets compressed due to  $M$ . Physically, peak values of  $M$  lead to the interpretation of the Lorentz force, which slows down the velocity. Furthermore, a low velocity profile is more progressive for SWCNTs/EG suspension.

Figure 5 explains the role of the thermal relaxation factor  $\alpha$  on the temperature profile  $\theta$ . The temperature field decreases for prominent values of  $\alpha$ . The thermal observations are deduced by varying  $\alpha$  for SWCNTs-MWCNTs/EG and SWCNTs/EG decomposition. Physically, higher values of  $\alpha$  are associated with the time required for the fluid to maintain its original position. The reduction in  $\theta$  is pronounced for SWCNTs-MWCNTs/EG. The results for observations of the thermal profile due to the Casson fluid parameter  $\gamma$  have been predicted in Figure 6.

The temperature profile  $\theta$  increases due to  $\gamma$ . However, the magnitude of the enhancement of  $\theta$  is slower. Moreover, the heat transfer improvement is superior for the hybrid nanofluid (SWCNTs-MWCNTs/EG).

Figure 7 presents comparative results for heat transfer subject to Casson fluid ( $Q_1=Q_2=0$ ), SWCNTs/EG. ( $Q_1=0.1$ ,  $Q_2=0$ ) (MWCNTs/EG ( $Q_1=0$ ,  $Q_2=0.1$ )) and SWCNTs-MWCNTs/EG ( $Q_1=Q_2=0.1$ ).

Heat transfer fluctuation is slower for the Casson fluid, while improved results for the thermal profile are associated ( $Q_1=Q_2=0.1$ ). Figure 8 aims to understand the behavior of  $\theta$  in view of the nanoparticles volume fraction  $Q_1$  and  $Q_2$ . Comparative observations are revealed for SWCNTs/EG and SWCNTs-MWCNTs/EG. The figure clearly indicates that  $\theta$  is enriched with variation of  $Q_1$  and  $Q_2$ . The improvement in heat transfer is maximum for SWCNTs-MWCNTs/EG as compared to SWCNTs/EG. In Figure 9, the results for the influence of Prandtl number  $Pr$  are shown against  $\theta$ . A larger change in  $Pr$  pronounced lower heat transfer for nanofluid and hybrid nanofluid. Physically, larger values of  $Pr$  correspond to low mass diffusivity, due to which  $\theta$  shows retarded trend. In order to evaluate the performance of heat source  $Q$  on  $\theta$ , Figure 10 has been prepared.

An increasing variation with larger  $Q$  is exhibited in the profile of  $\theta$ . The presence of a heat source provides extra energy to the system, which boosts the temperature profile. Figure 11 reflects the analysis for the radiation parameter  $R_d$  on  $\theta$ .

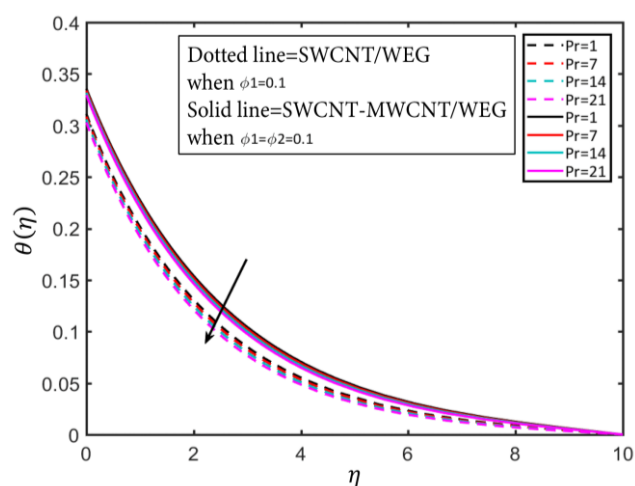


Figure 9. Temperature profile  $\theta$  for  $Pr$ .

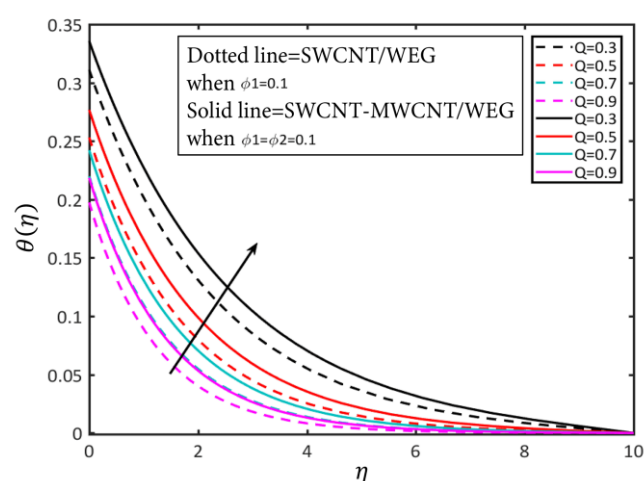


Figure 10. Temperature profile  $\theta$  for  $Q$ .

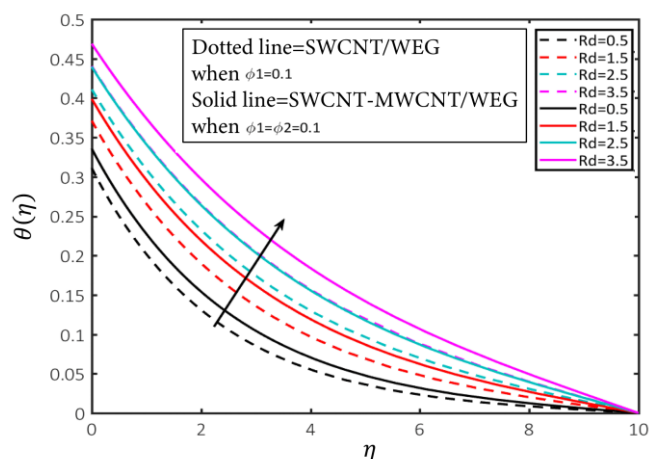


Figure 11. Temperature profile  $\theta$  for  $Rd$ .

Change in  $Rd$  leads to a boost in the temperature profile for both SWCNTs-MWCNTs/EG and SWCNTs/EG. The radiation phenomenon is associated with the transfer of energy through electromagnetic waves.

## 6. Conclusion

The heat transfer analysis with the utilization of Single-Walled (SW) and Multi-Walled (MW) carbon nanofluent with

Ethylene Glycol (EG) base fluid has been performed for a rotating disk. The significance of heat and radiative phenomena is addressed. The Cattaneo-Christov heat flux model is used to modify the heat equation. Comparative thermal observations for nanofluent Single-Walled Carbon Nano-Tubes/Ethylene Glycol (SWCNTs/EG) and hybrid nanofluent (SWCNTs-MWCNTs/EG) are investigated. The major results are summarized as:

- The radial velocity increases due to the stretching parameter for the nanofluent and hybrid nanofluent. However, the interaction of slip leads to a reduction in the velocity profile.
- A change in the thermal relaxation parameter leads to a decrement in the temperature profile for both SWCNTs/EG and SWCNTs-MWCNTs/EG suspensions.
- Heat transfer is enhanced for the Casson fluid parameter. The improvement in the thermal profile is prominent for the hybrid nanofluent.
- The fluctuation in heat transfer is more pronounced for the hybrid nanofluent as compared to the traditional nanofluent.
- Subject to increasing heat source and radiation parameter, the temperature profile increased.
- The heat transfer phenomenon increases for the nanoparticles' volume fraction of Single-Walled Carbon SWCNTs and Multi-Walled Carbon Nanotubes (MWCNTs). However, the improvement in thermal profile is dominant for MWCNTs.
- The modification in the current results can be suggested by studying the entropy generation analysis, bioconvection phenomenon and stability analysis.

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## Authors contribution statement

**First author:** Data curation; Formal analysis;

**Second author:** Methodology; Resources; Software;

**Third author:** Conceptualization; Data curation;

**Fourth author:** Formal analysis;

**Fifth author:** Investigation;

**Sixth author:** Project administration; Visualization;

**Seventh author:** Writing - original draft; Writing - review and editing.

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