Entropy optimization of non-Newtonian hybrid nanofluid flow with non-linear radiation, exponential and thermal-dependent heat source: Neuro-intelligent design A. Divya and P. Bala Anki Reddy\*

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### Abstract

The prediction of entropy generation with a thermal and exponential space dependent heat source of unsteady flow over a rotating disk is the artifact of the paper. For the specific physical model, Oldroyd-B within fluid flow is encrypted. Also, mechanism of cobalt and tantalum nanoparticles with in the blood is employed. The proper self-similarity variables are used to convert the non-linear PDE system of equations into an ODE form, which is then calculated using the Runge–Kutta 4<sup>th</sup> with shooting technique and artificial neural network. Visual representations are used to show how different skewing interact with each other. With a few exceptions, the research findings of the model are quite consistent with those reported in the literature. Skin frictions decrease for the parameters like radiation, Eckert number, Brinkman number and exponential based heat source. Nusselt number rises for electric and unsteady parameters. Also, entropy generation rises for magnetic field and Brinkman number whereas opposite tendency is observed for the electric field. Since cobalt stimulates red blood cell production, while tantalum is employed in bone implants and iodinated agents for blood imaging due to its long circulation time. Thus, this research may be used to treat anemia.

### **Keywords**

Electromagnetohydrodynamic flow; thermal and exponential space dependent heat source; Artificial Neural Network model; Oldroyd-B fluid; entropy generation.

# **1. Introduction**

In comparison to Newtonian materials, non-Newtonian materials have become more prevalent in the mechanical, commercial and industrial areas in recent decades. This is due to the fact that Newtonian fluids cannot predict elastic characteristics, but non-Newtonian fluids can possesses the highest viscoelastic property [1]. Mud, ketchup, glues, blood, fiber, mineral oils, ink, shampoos, chemical solutions, paints, exotic lubricants, cosmetics, annealing of copper wire, colloids and suspensions, clay coatings, coal water and a range of other thin and thick substances behave like non-Newtonian fluids and are treated as such kind [2,3]. Furthermore, such fluids are employed in synthetic processes, oil store construction, culinary products, material handling and in the multitude of different applications [4]. For the most part of non-Newtonian fluids, they are divided into three categories: differential, rate, and integral. The stress relaxation and creep processes are demonstrated by the fluids in rate type. One of that rate-type fluids is represented by the Oldroyd-B model, which is an extension of the upper convicted viscoelastic Maxwell fluid model with retardation time. Oldroyd-B [5] investigated this model of fluid. Actually, the progression of Oldroyd-B fluid is more suited to fit the rheological data rather than other non-Newtonian models, according to a literature review [6]. Khan et al. [7] investigated the Oldroyd-B fluid flow using Karman transformations to formulate the problem over a rotating disk. The investigation of OldroydB nanofluid with cross diffusion effects was did by Hayat et al. [7] and he discovered that the dufour effect enhances the thermal profile. Hafeez et al. [4] recently investigated Oldroyd-B fluid flow which is chemically reactive with Cattaneo–Christov heat flux theory over a rotating disk. Shiva kumara and Suresh Kumar [8] investigated Oldroyd-B fluid with the effects of flow and quadratic drag on the stability in a region of porous.

Chemical or nuclear processes generate heat energy within a body as an interior energy source/sink. Its significance may be observed in combustion research, heat exchangers, production of plastic, thermal insulation, fusion reactors, paper and steel manufacturing, nuclear reactors, among other things. The effects of an internal heat source/sink may be studied using two models. The first is a uniform temperature dependent internal heat source/sink process, while the second is a non-uniform space. In general, thermal based heat source(THS) has two dimensionless components which is encrypted in the energy equation, one for analyzing thermal based heat sources and the other for analyzing space based heat sources [9]. But these two models may not be able to accomplish more heat transmission in the fluid boundary layer, according to science. So, an exponential space-based heat source (ESHS) effect has been developed as a novel model for intensive heating processes in light of these findings. Khan et al. [10] studied irregular heat source with Marangoni convective flow over a disk which is rotating. Mahanthesh et al. [11] performed MHD flow with thermal and exponential space dependent heat source of SWCNT and MWCNT nanofluid over a rotating stretchable disk. Radiation on Maxwell fluid with in MWCNT nanotube was investigated by Fatehinasab et at. [12,13].

Entropy generation or production is the rate of heat transfer in any irreversible process. Usually, diffusion, Joule heating, chemical reactions, flow of heat through thermal resistance, fluid's viscosity, friction of solid surfaces are some of the irreversible processes that produce entropy. Although there are numerous reasons for entropy generation in this process, some of those can be named as heat exchange, fluid movement, mixing and expansion of substances, solid deformation, motion of bodies or any irreversible thermodynamic cycle. For example, heat pumps, air conditioners, heat engines, power plants and so on [10]. Jakeer and Reddy [14] investigated entropy generation of a hybrid nanofluid with EMHD stagnation point. Khan et al. [15] investigated the dynamics of MHD nanomaterial in three dimensional flow with entropy generation between two rotating disks. Rashidi et al. [16] explored the entropy generation of MHD steady flow owing to a spinning porous disk.

Several research on the uses of Artificial Neural Network in thermodynamics have been conducted in recent years. Reddy and Das [17] analyzed MHD boundary layer flow with chemical reaction employing a mix of artificial neural network modelling and numerical over a stretched cylinder. Raghu and Sriraam [18] explored the best configuration of a multilayer perceptron neural network classifier for detecting intracranial epileptic episodes. Hasan et al. [19] studied a heart disease related detection system through which Multi-Layer Perceptron neural network is used. Heidari et al. [20] developed a grasshopper optimization in the multilayer perceptron neural network for the hybrid.

To the best of the authors' knowledge, no research has been done on entropy generation in electromagnetohydrodynamic with a thermal and exponential space dependent heat source of unsteady flow over a rotating disk. The governing flow of non-linear partial differential equations are converted into a system of highly non-linear ordinary differential equations using appropriate similarity transformations, which are then numerically solved using a Runge–Kutta fourth order with shooting technique and then ANN is applied. To satisfy our criteria, we constructed the necessary graphs and tables for the established parameters. For this work, we used blood as the base fluid and nano particles like tantalum and cobalt to enhance Oldroyd-B fluid. The current study aims to be useful in clinical applications where tantalum is used as a nanoparticle that is easily oxidized in the air due to its high reactivity, as well as in the treatment of microbial infections and since cobalt nanoparticles are nontoxic at low concentrations [21] and have minimal side effects than antibiotics.

### 2. Formulation of the problem

Consider a non-Newtonian Oldroyd-B fluid over a rotating disk with an unsteady electromagnetohydrodynamic (EMHD) conducting flow of hybrid nanofluid where the disk is stretchable. Also, non-linear thermal radiation and exponential space-based heat source (ESHS) (irregular heat source/sink) is taken into an account. Here, disk rotates with an uniform magnetic field  $B_0$  and has the angular velocity  $\Omega$  which is placed at z = 0 as shown in Figure 1. The disk has a surface temperature termed as  $T_s$  and the temperature away from the disk as  $T_{\infty}$ . For the solvation of this problem, the following presumptions are used.

$$u = \frac{cr}{(1-bt)}, v = \frac{r\Omega}{(1-bt)}, B(t) = \frac{B_0}{(1-bt)^{\frac{1}{2}}}, T_s = T_0 - T_{ref} \left(\frac{r^2\Omega}{\nu(1-bt)^{\frac{3}{2}}}\right)$$
(1)

The equations for continuity, momentum and energy that govern this form of flow are as follows (Khan et al. [22], Hafeez et al. [23,24], Ahmad et al. [25]):

$$\frac{\partial w}{\partial z} + \frac{1}{r} \frac{\partial}{\partial r} (ur) = 0$$
<sup>(2)</sup>

$$\begin{pmatrix} \frac{\partial u}{\partial t} - \frac{v^2}{r} + w \frac{\partial u}{\partial z} + u \frac{\partial u}{\partial r} \end{pmatrix} = \upsilon_{hnf} \left( \frac{\partial^2 u}{\partial z^2} \right) - \lambda_1 \begin{bmatrix} u^2 \left( \frac{\partial^2 u}{\partial r^2} \right) + w^2 \frac{\partial^2 u}{\partial z^2} + 2uw \left( \frac{\partial^2 u}{\partial r \partial z} \right) - \frac{\partial^2 u}{\partial r \partial z} \\ \frac{2uv}{r} \left( \frac{\partial v}{\partial r} \right) - \frac{2vw}{r} \left( \frac{\partial v}{\partial z} \right) + \frac{uv^2}{r^2} + \frac{v^2}{r} \left( \frac{\partial u}{\partial r} \right) \end{bmatrix} + \\ \upsilon_{hnf} \lambda_2 \begin{bmatrix} -\frac{1}{r} \left( \frac{\partial u}{\partial z} \right)^2 - 2 \left( \frac{\partial u}{\partial z} \right) \left( \frac{\partial^2 w}{\partial z^2} \right) + w \left( \frac{\partial^3 u}{\partial z^3} \right) - \left( \frac{\partial u}{\partial r} \right) \left( \frac{\partial^2 u}{\partial z^2} \right) - \\ \left( \frac{\partial u}{\partial z} \right) \left( \frac{\partial^2 u}{\partial r \partial z} \right) + u \left( \frac{\partial^3 u}{\partial r \partial z^2} \right) \end{bmatrix} + w \left( \frac{\partial^3 u}{\partial r \partial z^2} \right) = \\ \frac{\sigma_{hnf} B_0}{\rho_{hnf} (1 - bt)} \left( E_0 - B_0 u \right) - \frac{\upsilon_{hnf}}{k^*} u$$

$$(3)$$

$$\begin{pmatrix} \frac{\partial v}{\partial t} + \frac{uv}{r} + w \frac{\partial v}{\partial z} + u \frac{\partial v}{\partial r} \end{pmatrix} = \upsilon_{hnf} \left( \frac{\partial^2 v}{\partial z^2} \right) - \lambda_1 \begin{bmatrix} u^2 \left( \frac{\partial^2 v}{\partial r^2} \right) + w^2 \left( \frac{\partial^2 v}{\partial z^2} \right) + 2uw \left( \frac{\partial^2 v}{\partial r \partial z} \right) + \\ \frac{2uv}{r} \left( \frac{\partial u}{\partial r} \right) + \frac{2vw}{r} \left( \frac{\partial u}{\partial z} \right) - 2 \frac{u^2 v}{r^2} - \frac{v^3}{r^2} \\ + \frac{v^2}{r} \left( \frac{\partial v}{\partial r} \right) \\ + \frac{v^2}{r} \left( \frac{\partial v}{\partial r} \right) \\ - \frac{1}{r} \left( \frac{\partial u}{\partial z} \right) \left( \frac{\partial v}{\partial z} \right) - \left( \frac{\partial v}{\partial r} \right) \left( \frac{\partial^2 u}{\partial z^2} \right) + w \left( \frac{\partial^3 v}{\partial z^3} \right) \\ + \frac{\sigma_{hnf} B_0}{\rho_{hnf} (1 - bt)} (E_0 - B_0 v) - \frac{v_{hnf}}{k^*} v \\ \frac{v}{r} \left( \frac{\partial^2 u}{\partial z^2} \right) - \left( \frac{\partial v}{\partial z} \right) \left( \frac{\partial^2 u}{\partial r \partial z} \right) - \frac{u}{r} \left( \frac{\partial^2 v}{\partial z^2} \right) \\ + \frac{\mu_{hnf}}{(\rho c_p)_{hnf}} \left[ \left( \frac{\partial u}{\partial z} \right)^2 + \left( \frac{\partial v}{\partial z} \right)^2 \right] \\ - \frac{16}{3} \frac{\sigma^*}{k^* (\rho c_p)_{hnf}} \frac{\partial}{\partial z} (T^3 \frac{\partial T}{\partial z}) + \frac{Q_r^*}{(\rho c_p)_{hnf}} (T - T_0) + \frac{Q_r^* (T_s - T_0)}{(\rho c_p)_{hnf}} \exp(-n\sqrt{\frac{\Omega}{v}} z) + \\ (5) \\ - \frac{\sigma_{hnf}}{(\rho c_p)_{hnf} (1 - bt)} [E_0^2 + B_0^2 (u^2 + v^2)] \end{cases}$$

The Rosseland approximation may be used to represent the radiative heat flux, where  $\sigma^*$  and  $k^*$  are the Stefan Boltzmann and mean absorption coefficients, respectively.

$$q_r = -\frac{4\sigma^*}{3k^*}\frac{\partial T^4}{\partial z} = -\frac{16\sigma^*T^3}{3k^*}\frac{\partial T}{\partial z}$$
(6)

The following are the similarity transformations:

$$u = \frac{r\Omega}{(1-bt)} f'(\eta), \quad v = \frac{r\Omega}{(1-bt)} g(\eta), \quad w = -2 \left(\frac{\upsilon\Omega}{(1-bt)}\right)^{\frac{1}{2}} f(\eta), \quad \eta = \sqrt{\frac{\Omega}{\upsilon(1-bt)}} \quad z,$$

$$T = T_0 - T_{ref} \frac{r^2\Omega}{\upsilon(1-bt)^{\frac{3}{2}}} \theta(\eta) \quad . \tag{7}$$

The boundary conditions are as follows:

$$u = \frac{cr}{1 - bt}, v = \frac{r\Omega}{1 - bt}, w = 0, T = T_s \qquad \text{at } z = 0$$

$$\frac{\partial u}{\partial z} = 0, u \to 0, \quad \frac{\partial v}{\partial z} = 0, v \to 0, T \to T_0 \qquad \text{as } z \to \infty$$
(8)

The non-linear dimensionless equations are as follows:

$$\left(\frac{N_{1}}{N_{3}}\right)\beta_{2}(2f''^{2}-2ff'') + \left(\frac{N_{1}}{N_{3}}\right)f''' - \beta_{1}(4fgg'+4f^{2}f'''-4ff'f'') - S(\frac{\eta}{2}f''+f') 
+ (g^{2}+2ff''-f'^{2}) - \left(\frac{N_{1}}{N_{3}}\right)\beta f' + \left(\frac{N_{2}}{N_{3}}\right)M(E_{1}-f') = 0$$

$$\left(\frac{N_{1}}{N_{3}}\right)\beta_{2}(2g'f''-2fg''') - \beta_{1}\left(4f'^{2}g+4f^{2}g''-4ff'g'-4ff'g) 
-S(\frac{\eta}{2}g'+g) - 2(g'f-f'g) + \left(\frac{N_{1}}{N_{3}}\right)g'' - \left(\frac{N_{1}}{N_{3}}\right)\beta g + \left(\frac{N_{2}}{N_{3}}\right)M[E_{1}-g] = 0$$

$$\left(\frac{N_{4}}{N_{4}}\right)\theta'' + Rd\left(\frac{1}{N_{4}}\right)\left(\frac{4}{N_{4}}\right)\left[\frac{\theta''+(\theta_{w}-1)^{3}(3\theta^{2}\theta'^{2}+\theta^{3}\theta'')}{+3(\theta_{4}-1)^{2}(2\theta\theta'^{2}+\theta^{2}\theta'')}\right] + \left(\frac{N_{1}}{N_{4}}\right)Pr Ec(f''^{2}+g'^{2})$$
(9)

$$\left(\frac{N_4}{N_5}\right)\theta'' + Rd\left(\frac{1}{N_5}\right)\left(\frac{4}{3}\right)\left\{+3(\theta_w - 1)^2(2\theta\theta'^2 + \theta^2\theta'') + 3(\theta_w - 1)(\theta'^2 + \theta\theta'')\right\} + \left(\frac{N_1}{N_5}\right)\Pr Ec(f''^2 + g'^2) + 2\Pr \left(f\theta' - \theta f'\right) - S\Pr \left(\frac{3}{2}\theta + \frac{\eta}{2}\theta'\right) + \left(\frac{N_2}{N_5}\right)M Ec\Pr \left(f'^2 + g^2 + E_1^2\right) + \left(\frac{1}{N_5}\right)\Pr Q_t \theta + \left(\frac{1}{N_5}\right)\Pr Q Exp(-n\xi) = 0$$
(11)

With the boundary conditions as:

$$f' = \omega, g = 1, f = 0, \theta = 1, \qquad \text{at } \eta = 0$$

$$f'' \to 0, g \to 0, g' \to 0, \theta \to 0 \qquad \text{as } \eta \to \infty$$
(12)

The dimensionless parameters are as:

$$\begin{split} S &= \frac{b}{\Omega} \ , \ \omega = \frac{c}{\Omega} \ , \ \beta = \frac{\upsilon(1-bt)}{k^*\Omega}, \ \Pr = \frac{\mu_f(C_p)_f}{k_f}, \ \beta_1 = \frac{\lambda_1\Omega}{1-bt}, \ \beta_2 = \frac{\lambda_2\Omega}{1-bt}, \ Rd = \frac{4\sigma^*T_0^3}{k^*k_f}, \\ \theta_w &= \frac{T_s}{T_0}, \qquad Ec = \frac{r^2\Omega^2}{(1-bt)^2(\Delta T)(C_p)_f}, \qquad Q = \frac{Q_E^*(1-bt)}{(\rho c_p)\Omega}, \ \xi = z\sqrt{\frac{\Omega}{\upsilon}}, \qquad M = \left(\frac{\sigma_f B_0^2}{\rho_f\Omega}\right), \\ Q_t &= \frac{Q_T^*(1-bt)}{(\rho c_p)\Omega}, \qquad N_1 = \frac{\mu_{hnf}}{\mu_f}, \qquad N_2 = \frac{\sigma_{hnf}}{\sigma_f}, \qquad N_3 = \frac{\rho_{hnf}}{\rho_f}, \qquad N_4 = \frac{k_{hnf}}{k_f}, \qquad N_5 = \frac{(\rho C_p)_{hnf}}{(\rho C_p)_f}, \\ E_1 &= \left(\frac{E_0(1-bt)}{r\Omega B_0}\right). \end{split}$$

# 3. Engineering interest quantities

The skin friction of both the velocities are defined as follows:

$$C_{f} = \frac{\tau_{w1}(1-bt)^{2}}{\rho_{f}(r\Omega)^{2}}$$
(13)

$$C_{g} = \frac{\tau_{w2} (1 - bt)^{2}}{\rho_{f} (r\Omega)^{2}}$$
(14)

Here, 
$$\tau_{w1} = \mu_{hnf} \left(\frac{\partial u}{\partial z}\right)_{z=0}, \quad \tau_{w1} = \mu_{hnf} \left(\frac{\partial v}{\partial z}\right)_{z=0}$$
  

$$\operatorname{Re}_{x}^{\frac{1}{2}} C_{f} = N_{1} f''(0) \qquad (15)$$

$$\operatorname{Re}_{x}^{\frac{1}{2}}C_{g} = N_{1}g'(0) \tag{16}$$

The heat transfer rate, often known as the Nusselt number, is the physical quantity of concern in this subject.

$$Nu_r = \frac{rq_w}{k_f (T_s - T_0)} \tag{17}$$

Where  $q_w = (-k_{hnf}(\frac{\partial T}{\partial z})_{z=0}) + (\frac{16\sigma^* T_{\infty}^3}{3k^* k_f})_{z=0}$ 

$$Nu_{x} \operatorname{Re}_{x}^{\frac{-1}{2}} = -\left\{ N_{4} + \frac{4}{3} Rd[1 + (\theta_{w} - 1)\theta(0)]^{3} \right\} \theta'(0)$$
(18)

Where  $\operatorname{Re}_{x}$  is the local Reynolds number and it can be written as,

$$\operatorname{Re}_{x} = \left(\frac{r^{2}\Omega}{\upsilon(1-bt)}\right)$$

## 4. Exploration of Entropy generation

Within the influences of electric and magnetic forces, the phrase for volumetric entropy generation number is given as follows (Khan et al. [15], Rashidi et al. [16], Mumraiz et al. [26], Reddy [27]):

$$S_{gen}^{\prime\prime\prime} = \frac{k_{hnf}}{T_0^2} \left[ \left( \frac{\partial T}{\partial z} \right)^2 + \frac{16\sigma^* T_0^3}{3k^* k_{hnf}} \left( \frac{\partial T}{\partial z} \right)^2 \right] + \frac{\mu_{hnf}}{T_0} \left[ \left( \frac{\partial u}{\partial z} \right)^2 + \left( \frac{\partial v}{\partial z} \right)^2 \right] + \frac{\sigma_{hnf}}{T_0(1-bt)} [E_0^2 + B_0^2(u^2 + v^2)]$$

$$(19)$$

The conduction, viscosity, and joule effects are all included in the above equation. The first term in the above formula exhibits irreversibility through heat conduction. The irreversibility produced by frictional effects is represented by the second term and the corresponding joule dissipation involving the magnetic and electric fields is represented by the third term. The

entropy generation number can be stated as the dimensionless counterpart of the entropy generation rate, which is the ratio of the actual and characteristic entropy generation rates. So, the reduced entropy generation number equation can be written as follows:

$$N_{G} = \alpha_{1} \left\{ N_{4} + \frac{4}{3} Rd(1 + \theta(\theta_{w} - 1))^{3} \right\} \theta'^{2} + N_{1} Br(f''^{2} + g'^{2}) + N_{2} M Br\left\{ E_{1}^{2} + f'^{2} + g^{2} \right\}$$
(20)

Here, the dimensionless parameters are given below:

$$N_{G} = \frac{T_{0} S_{gen}^{'''} \upsilon(1-bt)}{k_{f} \Omega \Delta T}, \quad \Delta T = (T_{s} - T_{0}), \quad \alpha_{1} = \frac{\Delta T}{T_{0}}, \quad Br = \frac{\mu_{f} r^{2} \Omega^{2}}{k_{f} (T_{s} - T_{0})(1-bt)^{2}}.$$

But the entropy generation number is inadequate to overcome the difficulty like, the dominance of irreversibility mechanisms which is physically significant. To comprehend entropy generation methods, the Bejan number is used, which is the ratio of entropy generation owing to heat transfer to overall entropy generation.

$$Be = \frac{\alpha_1 \left\{ N_4 + \frac{4}{3} Rd(1 + \theta(\theta_w - 1))^3 \right\} \theta'^2}{\alpha_1 \left\{ N_4 + \frac{4}{3} Rd(1 + \theta(\theta_w - 1))^3 \right\} \theta'^2 + N_1 Br(f''^2 + g'^2)}$$
(21)

Table 1 values and the quantities are used to get the output of the program in MATLAB. The hybrid nanofluid quantities are defined as,

Dynamic viscosity: 
$$\mu_{hnf} = \frac{\mu_f}{(1 - \phi_{Ta})^{2.5} (1 - \phi_{Co})^{2.5}}$$
 (22)

$$\rho_{hnf} = \rho_f (1 - \phi_{Co}) [(1 - \phi_{Ta}) + \phi_{Ta} (\frac{\rho_{Ta}}{\rho_f})] + \phi_{Co} (\rho_{Co})$$
(23)

$$(\rho c_p)_{hnf} = (\rho c_p)_f (1 - \phi_{Co})(1 - \phi_{Ta}) + \phi_{Ta}(\rho c_p)_{Ta} + \phi_{Co}(\rho c_p)_{Co}$$
(24)

Electrical conductivity:  $\frac{\sigma_{hnf}}{\sigma_{bf}} = \left(\frac{(1+2\phi_{Co})\sigma_{Co} + 2(1-\phi_{Co})\sigma_{bf}}{(1-\phi_{Co})\sigma_{Co} + (2+\phi_{Co})\sigma_{bf}}\right)$ 

where, 
$$\frac{\sigma_{bf}}{\sigma_f} = \left(\frac{(1+2\phi_{Ta})\sigma_{Ta} + 2(1-\phi_{Ta})\sigma_f}{(1-\phi_{Ta})\sigma_{Ta} + (2+\phi_{Ta})\sigma_f}\right)$$
(25)

Thermal conductivity:  $\frac{k}{k}$ 

Density:

Heat capacity:

$$\frac{k_{hnf}}{k_{bf}} = \left(\frac{(1+2\phi_{Co})k_{Co} + 2(1-\phi_{Co})k_{bf}}{(1-\phi_{Co})k_{Co} + (2+\phi_{Co})k_{bf}}\right)$$

where, 
$$\frac{k_{bf}}{k_f} = \left(\frac{(1+2\phi_{Ta})k_{Ta}+2(1-\phi_{Ta})k_f}{(1-\phi_{Ta})k_{Ta}+(2+\phi_{Ta})k_f}\right)$$
 (26)

### **5.** Method of solution

# 5.1. Runge-Kutta(RK) 4<sup>th</sup> order method

A boundary value issue is formed by the Equations 9 - 11 and the boundary conditions of Equation 12. Entropy generation Equation 20 and Bejan number Equation 21 are also converted as a result of this. The shooting technique is used to solve these equations by transforming them to an initial value problem. For this, we convert the above-mentioned non-linear ordinary differential equations to a system of first-order differential equations as follows:

$$\begin{split} f &= \wp_1, \ f' = \wp_2, \ f'' = \wp_3, \ f''' = \wp_4, \ f^{iv} = \wp_4', \ g &= \wp_5, \ g' = \wp_6, \ g'' = \wp_6', \ \theta &= \wp_8, \ \theta' = \wp_9, \\ \theta'' &= \wp_9'. \\ & \left\lceil 2(n_1/n_3)\beta_2\wp_3^2 - \beta_1(4\wp_1\wp_5\wp_6 + 4\wp_1^2\wp_4 - 4\wp_1\wp_2\wp_3) + \right\rceil \end{split}$$

$$\wp_{4}' = \begin{bmatrix} 2(n_{1}/n_{3})\beta_{2}\wp_{3}^{2} - \beta_{1}(4\wp_{1}\wp_{5}\wp_{6} + 4\wp_{1}^{2}\wp_{4} - 4\wp_{1}\wp_{2}\wp_{3}) + \\ (n_{1}/n_{3})\wp_{4} + (n_{2}/n_{3})M(E_{1} - \wp_{2}) - (n_{1}/n_{3})\beta\wp_{2} - \\ S(\wp_{2} + (\eta/2)\wp_{3} + (\wp_{5}^{2} + 2\wp_{1}\wp_{3} - \wp_{2}^{2}) \\ 2(n_{1}/n_{3})\beta_{2}\wp_{1} \end{bmatrix}$$

$$(27)$$

$$\wp_{7}^{\prime} = \begin{bmatrix} 2(n_{1}/n_{3})\beta_{2}\wp_{3}\wp_{6} - \beta_{1}(4\wp_{2}^{2}\wp_{5} + 4\wp_{1}^{2}\wp_{7} - 4\wp_{1}\wp_{2}\wp_{6} - 4\wp_{1}\wp_{3}\wp_{5}) + (n_{1}/n_{3})\wp_{7} + \\ (n_{2}/n_{3})M(E_{1} - \wp_{5}) - (n_{1}/n_{3})\beta_{5}\wp_{5} - S[(\eta/2)\wp_{6} + \wp_{5}] - 2(\wp_{2}\wp_{5} - \wp_{6}\wp_{1}) \\ 2(n_{1}/n_{3})\beta_{2}\wp_{1} \end{bmatrix}$$
(28)

$$\wp_{9}' = - \begin{pmatrix} (4/3)(Rd/n_{5})[(Tw-1)^{3}(3\wp_{8}^{2}\wp_{9}^{2}) + 3(Tw-1)^{2}(2\wp_{8}\wp_{9}^{2}) \\ +3(Tw-1)(\wp_{9}^{2})] + (n_{1}/n_{5})Ec \operatorname{Pr}(\wp_{3}^{2} + \wp_{6}^{2}) + \\ 2\operatorname{Pr}(\wp_{1}\wp_{9} - \wp_{8}\wp_{2}) - S\operatorname{Pr}[(3/2)\wp_{8} + (\eta/2)\wp_{9}] + \\ (\operatorname{Pr}/n_{5})Qe \operatorname{Exp}(-n\xi) + (\operatorname{Pr}/n_{5})Qt \wp_{8} \\ + (n_{2}/n_{5})MEc \operatorname{Pr}(\wp_{2}^{2} + \wp_{5}^{2} + E_{1}^{2}) \\ (n_{4}/n_{5}) + (Rd/n_{5})(4/3) \\ [1 + (Tw-1)^{3}\wp_{8}^{3} + 3(Tw-1)^{2} \\ \wp_{8}^{2} + 3(Tw-1)\wp_{8}] \end{cases}$$
(29)

Now the boundary conditions as,

$$\wp_{1}(0) = 0, \quad \wp_{2}(0) = \omega, \quad \wp_{5}(0) = 1, \quad \wp_{8}(0) = 1,$$
  
$$\wp_{2}(\infty) = 0, \\ \wp_{3}(\infty) = 0, \\ \wp_{5}(\infty) = 0, \\ \wp_{6}(\infty) = 0, \\ \wp_{8}(\infty) = 0$$
(30)

Followed by the entropy generation and Bejan number as shown below:

$$N_{G} = \alpha_{1} \left\{ n_{4} + (4/3)(Rd) [1 + \wp_{8}(Tw - 1)]^{3} \right\} \wp_{9}^{2} + n_{1} Br(\wp_{3}^{2} + \wp_{6}^{2}) + n_{2} M Br(E_{1}^{2} + \wp_{2}^{2} + \wp_{5}^{2})$$
(31)

$$Be = \frac{\alpha_1 \left\{ n_4 + (4/3)(Rd)[1 + \wp_8(Tw-1)]^3 \right\} \wp_9^2}{\alpha_1 \left\{ n_4 + (4/3)(Rd)[1 + \wp_8(Tw-1)]^3 \right\} \wp_9^2}$$
(32)  
+  $n_1 Br(\wp_3^2 + \wp_6^2) + n_2 M Br(E_1^2 + \wp_2^2 + \wp_5^2)$ 

The values of  $\beta_4(0)$ ,  $\beta_7(0)$  and  $\beta_9(0)$  i.e., f''(0), g''(0) and  $\theta'(0)$  is required to integrate Equation 27 - 29 as an initial value problem, but such kind of values are not furnished at the boundary. So, the appropriate guess values are picked and then the integration process is performed. The selection of a suitable finite value of  $\eta$  at  $\infty$  is the most critical aspect of the shooting procedure. To find  $\eta$  at  $\infty$  for the boundary value issue, we start with some initial estimate values for a certain set of physical parameters, culminating in obtain f'''(0), g''(0) and  $\theta'(0)$ . The operation is repeated with another enormous values of  $\eta$  at  $\infty$  until two consecutive values of f''(0), g''(0) and  $\theta'(0)$  differ only by one significant digit. The most acceptable value of the limit  $\eta$  at  $\infty$  for that specific collection of parameters is eventually chosen as the last value of  $\eta$  at  $\infty$ . For a different set of physical factors, the value of  $\eta$  at  $\infty$  may change. The integration begins once the finite value of  $\eta$  at  $\infty$  has been determined. Adjust the estimated values f''', g'' and  $\theta'$  to offer a better approximation to the solution by comparing the computed values for f', g and  $\theta$  at  $\eta = 8$ (say) with the specified boundary conditions f'(8) = 0, g(8) = 0 and  $\theta(8) = 0$ . We use the fourth order Runge-Kutta technique with a step size of h = 0.01 to apply the series values for  $f'''(0), g''(0), \theta'(0)$ . The technique is continued until the findings have converged to the required degree of accuracy of  $10^{-8}$ .

Through this method the values of skin friction coefficients and Nusselt number for different parameters like M,  $\beta_1$ ,  $\beta_2$ ,  $E_1$ , Rd, Ec, Pr, S, Q, Br and  $\alpha_1$  is dragged and then ANN is used for comparison and as well as to plot the output. The Table 2 gives the comparison of f'(0) for rotation parameter in R-K 4<sup>th</sup> order method which is performed in the MATLAB.

## 5.2.1. Artificial Neural Network (MLP-NN)

ANNs are built in the same way that human and animal brains are built. Basic scalar messages, simple processing components, a high degree of interconnection and adoptive interaction between units are the things which make them a type of multi-processor computer system [31]. Actually, ANN provides a reasonably quick and flexible way of modelling, so it is appropriate for rainfall-runoff prediction [32,33]. Layers of neurons make up an ANN. One or more hidden layers of neurons connect the input layer of neurons to the output layer of neurons. The interconnecting link between the neuron layers is made up of connection weights. This method changes its weights throughout the training phase to reduce the errors between the projected result and the actual output using the Back Propagation algorithm [34]. To get the best topology and weights, ANN is trained using experimental data and then evaluated with more experimental data whereas, bias refers to the weight that is provided directly to one neuron without being coupled to the prior neuron in specific circumstances. The most common type of ANN is the multilayer perceptron (MLP). It also has one or more hidden layers feed forward neural network. The sigmoid function was chosen as the activation function.

$$f(s) = \frac{1}{1 + e^{-s}}$$
(33)

Where,  $s_i = \sum_{i=1}^{n} W_i x_i$ , in which the term  $W_i$  is related to weights and  $x_i$  for input values. In the next part, we'll go through the ANN implementation in more detail as we go over the learning methods.

#### **5.2.2. Levenberg Marquardt Algorithm(LM-NN)**

Levenberg Marquardt is the first learning algorithm to be implemented. LM is a fastconverging training technique that has a lot of applications in neural network discipline [35]. It's a variant of the standard Newton algorithm for determining the optimum answer to a minimization issue [36].

Two-layered neural networks with specific variables and parameters are shown in Figure 2. Here, indication of  $P_n$  is for input,  $W_{(i,j)}$  for the first layer's connecting weight,  $V_{(i,j)}$  for the second layer's connecting weight, and  $q_n$  for the output.

$$a(i) = \sum_{i=1}^{n} W_{(i,j)} P_i$$
(34)

The second layer's net output from unit i is as follows:

$$q(i) = \sum_{i=1}^{n} f(a(h))V_{(i,j)}$$
(35)

The goal of ANN is to figure out how input and output pairs are connected. The hidden unit is named as h, and the activation function is as f(). The Sigmoid function was chosen as the activation function.

$$f(s) = \frac{1}{1 + e^{-s}}$$
(36)

The Gauss-Newton technique provides an update.

$$\Delta x = [J^{T}(x)J(x)]^{-1}J^{T}(x)e(x)$$
(37)

while Levenberg Marquardt's to the Gauss-Newton technique is such that

$$\Delta x = [J^{T}(x)J(x) + \mu I]^{-1}J^{T}(x)e(x)$$
(38)

When the scalar  $\mu$  is 0, Eq. (38) is just Newton's technique; however, when the scalar  $\mu$  is large, Eq. (33) becomes gradient descent with a short step size. The original description of Levenberg-Marquardt is explained in [37].

By incorporating information as input and calculating outputs, from different node activations and interconnection weights, this is how the output of ANN was calculated through the LM-NN method. The mean percentile error was computed after comparing the output to the experimental output. The error value was then transmitted backwards through the network and the weights at each node in each layer were adjusted accordingly. The method was then performed iteratively until the total error value fell below a predefined

threshold. As shown in Figure 3, the eleven parameters (M,  $\beta_1$ ,  $\beta_2$ ,  $E_1$ , Rd, Ec, Pr, S, Q, Brand  $\alpha_1$ ) that were obtained for the samples utilized in the research were used as input nodes, and three parameters (skin friction coefficients in xz and yz directions and Nusselt number) of these samples were employed as the ANN's output parameters. The method was then performed iteratively until the total error value fell below a predefined threshold. The numerical values acquired for all of the parameters in R-K 4<sup>th</sup> order method as shown in Tables 3, 4 and 5 were utilized to train the ANN in this research. Also the following flow chart Figure 4, gives the sketch of how the output extraction is done through two methods. MPE value for this rate of heat trnasfer is (0.0034). MPE means mean percentile error for the  $Cf_r \operatorname{Re}_r^{1/2}$  is (0.9787) and for the  $Cg_r \operatorname{Re}_r^{1/2}$  is (0.9337).

### 6. Results ans discussion

Numerical consequences performed for skin friction along x and y directions and Nusselt number are illustrated in this section through MATLAB and then ANN method of Levenberg Marquardt is used to compare the results. Also, the graphs of this parameters are performed by using ANN method. In MATLAB the results are gained for the accompanying fixed parametric values: S = 0.3, M = 0.5,  $\beta_1 = 0.3$ ,  $\beta_2 = 0.3$ ,  $E_1 = 0.5$ , Rd = 1.0, Ec = 0.05, Q = 0.3,  $\alpha = 0.2$ , and  $Q_t = 0.2$ . Actually, LM-NN is divided into three phases: training, validation, and testing. The activation function of artificial neurons was a sigmoid function and training was completed with a predetermined 176 number of epochs. The ANN model for the skin friction coefficients and Nusselt number was trained, validated and tested using a total of 44 numerical results. The training set consisted of 34 data sets, while the validation set consisted of 7 data sets and the balance of the data was utilised to evaluate the model's findings. Figures 5 and 6 show the skin friction coefficient of  $Cf_r \operatorname{Re}_x^{1/2}$  and  $Cg_r \operatorname{Re}_x^{1/2}$  whereas Figure 7 explores the Nusselt number for the proposed ANN model's training, validation, and test sets, respectively. This section shows the numerical results of skin friction coefficients ( $Cf_r \operatorname{Re}_x^{1/2}$  and  $Cg_r \operatorname{Re}_x^{1/2}$ ), as well as the Nusselt number ( $Nu_x \operatorname{Re}_x^{-1/2}$ ).

For all data sets, the model's MPE values were 0.9787, 0.9337, and 0.0034, respectively. Because they replicate complex relationships between input and output variables, the ANN models seem to have been effectively trained. Furthermore, the projected skin friction coefficients and Nusselt number values from the ANN model are compared to numerically obtained skin friction coefficients and Nusselt number values for the training, validation, and test sets, as shown in Figures 5, 6 and 7, respectively. The ANN model's conclusions are quite similar to the numerical results. So far, our study has proven that the ANN can accurately simulate skin friction coefficients and the Nusselt number. The numerical findings and the ANN(LM-NN) model's conclusions are very comparable.

From the Figure 8, it is noticed that for the higher values of Eckert number and radiation parameters, the skin friction coefficient  $Cf_r \operatorname{Re}_x^{1/2}$  will decline automatically. Similarly, when the Brinkman number and temperature ratio parameter intensify,  $Cf_r \operatorname{Re}_x^{1/2}$  decreases, as seen in Figure 9. It is evident that from the Figure 10, that skin friction coefficient  $Cf_r \operatorname{Re}_x^{1/2}$  declines for the higher values of the parameters Q and Pr. Figure 11 shows the

decreasing tendency of  $Cg_r \operatorname{Re}_x^{1/2}$  for increasing parameters Brinkman number and temperature ratio parameter. Also,  $Cg_r \operatorname{Re}_x^{1/2}$  declines for the higher values of the parameters Q and Pr which is illustrated in the Figure 12.

Figure 13 demonstrates that for the higher values of electric field and unsteady parameters is observed to be inclined for the rate of heat transfer  $Nu_x \operatorname{Re}_x^{-1/2}$ . For the parameter values of Deborah number and magnetic field on Nusselt number is explored in the Figure 14. But it is seen from the Figure 13 that for those parameters Nusselt number  $Nu_x \operatorname{Re}_x^{-1/2}$  declines as those parameters increases.

From the MATLAB, Figures 15-18 is extracted on entropy generation parameter. Figure 15 shows how the entropy generation intensifies as the magnetic field strength increases. Physically, increasing the Lorentz force by increasing the magnetic parameter creates greater friction, which increases the rate of entropy generation. As seen in Figure 16, the entropy production rate reduces as the electric field intensity increases. Figure 17 shows that the entropy production rate increases as the Brinkman number increases. Because viscous effects have gotten greater with the growth in Brinkman numbers, this condition in the entropy generating rate outcomes has arisen. The entropy generation rises for the greater values of the temperature ratio parameter is observed from the Figure 18.

## 7. Main findings

The numerical modelling and ANN(LM-NN) model results are quite close to the numerical findings. As a result of the present study's results, the suggested ANN model is successful for EMHD boundary layer slip flow over a rotating disk embedded in a porous medium with Oldroyd-B fluid. Also, PDEs are converted to ODEs using the relevant conversions. The reference set is generated using the R-K 4<sup>th</sup> order approach with the shooting methodology and then generated by using ANN(LM-NN) method for varying relevant parameters values. The major output drawn from this study can be summarized as below:

- Skin friction coefficients decreases for the higher values of Eckert number and radiation parameters.
- The rate of heat transfer declines for the rise in magnetic and Deborah number parameters.
- ➡ For the rise in the parameters like Brinkman number, Prandtl number and temperature ratio parameter, both the skin frictions will decline.
- Heat transfer increases with increasing in electric and unsteady parameters.
- Entropy generation rises for magnetic field, Brinkman number and temperature ratio parameter.
- **4** Increase in the electric field parameter, entropy generation declines.

This current therapeutic model will be very interesting to clinicians for the treatment of anemia as well as in the treatment of microbial infections etc. Since we considered tantalum and cobalt as nanoparticles in which tantalum is utilized in bone implants and iodinated agents for blood imaging because of its longer circulation time. Cobalt is a component of vitamin B12, which stimulates red blood cell formation.

List of symbols									
$r, \varphi, z$	are the cylindrical coordinates								
u, v, w	are the velocity components								
f	is the axial velocity field								
f'	is the radial velocity field								
g	is the azimuthal velocity field								
Т	is the temperature of the fluid								
S	is the measure of unsteadiness								
М	is the Magnetic field parameter								
$B_0$	is the uniform magnetic field								
$T_s$	is the surface temperature								
$T_0$	is the origin temperature								
$T_{ref}$	is the constant reference temperature								
Re	is the Local Reynolds number								
Ec	is the Eckert number								
Pr	is the Prandtl number								
Rd	is the thermal radiation								
$N_{G}$	is the Local entropy generation								
$Cf_r \operatorname{Re}_x^{1/2}$	is the skin friction co-efficient of $f$ velocity								
$Cg_r \operatorname{Re}_x^{1/2}$	is the skin friction co-efficient of g velocity								
$Nu_x \operatorname{Re}_x^{-1/2}$	is the Local Nusselt number								
Be	is the Bejan number								
$N_1, N_2, N_3, N_4, N_5$	are the hybrid nanofluid constants								
k	is the thermal conductivity								
$Q_{\scriptscriptstyle T}^*$	is the thermal-dependent heat source coefficient								
$Q_{\scriptscriptstyle E}^*$	is the exponential space-dependent heat source coefficient								
n	is the exponential index								
С	is the stretching rate								
Q	is the exponential based heat source parameter								
$Q_t$	is the thermal space dependent heat source parameter								
	Greek symbols								
ρ	is the fluid density								
υ	is the kinematic viscosity								
μ	is the dynamic viscosity								
σ	is the electric conductivity								
η	is the dimensionless variable								
<i>k</i> *	is the mean absorption co-efficient								
$\sigma^*$	is the Stefan Boltzmann constant								
θ	is the dimensionless temperature								
$\phi_{Ta}$	is the volume fraction of tantalum								

$\phi_{Co}$	is the volume fraction of Cobalt
Ω	is the angular velocity
$\lambda_1$	is the relaxation time parameter
β	is the Porosity parameter
$\beta_1, \beta_2$	are the Deborah numbers
$\theta_{_W}$	is the temperature ratio parameter
$\alpha_1$	is the temperature difference parameter
ω	is the rotation parameter
	Subscripts
f	represents the fluid
nf	represents the nanofluid
hnf	represents the hybrid nanofluid

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Figure 1. Geometry of the problem.

Figure 2. Neural network with two-layered hidden neuron.















**Figure 6.** Graphical representation of the skin friction coefficient ( $Cg_r \operatorname{Re}_x^{1/2}$ ).



**Figure 7.** Graphical representation of the Nusselt number( $Nu_x \operatorname{Re}_x^{-1/2}$ ).





**Figure 8.** Sway of *Ec* and *Rd* on  $Cf_r \operatorname{Re}_x^{1/2}$ .

**Figure 9.** Sway of *Br* and  $\alpha_1$  on  $Cf_r \operatorname{Re}_x^{1/2}$ .





**Figure 10.** Sway of Q and Pr on  $Cf_r \operatorname{Re}_x^{1/2}$ .







**Figure 12.** Sway of Q and Pr on  $Cg_r \operatorname{Re}_x^{1/2}$ .







**Figure 14.** Sway of  $\beta_1$  and *M* on  $Nu_x \operatorname{Re}_x^{-1/2}$ .

**Figure 15.** Sway of M on  $N_G$ .



**Figure 16.** Sway of  $E_1$  on  $N_G$ .



**Figure 17.** Sway of Br on  $N_G$ .



**Figure 18.** Sway of  $\alpha_1$  on  $N_G$ .



**Table 1.** Thermophysical properties of hybrid nanofluid.

Physical properties	Blood	Tantalum (Ta)	Cobalt (Co)
$\rho(kgm^{-3})$	3617	16650	8900
$C_p(J(kg)^{-1}K^{-1})$	1050	140	445
$k(W(m^{-1}K^{-1}))$	0.52	57	100
$\sigma(\Omega m)^{-1}$	1.33	$7.7 \times 10^{6}$	$1.7 \times 10^{7}$
Pr	21		

**Table 2.** Comparison of f'(0) for various values of  $\omega$ .

Variation of $\omega$	Uddin et al. [28]	Mustafa et al. [29]	Ahmed et al. [30]	Present
0	-1.1740	-1.1737	-1.1739	-1.1734
1	-0.9485	-0.9483	-0.9484	-0.9488
2	-3265	-3263	-3264	-3248
-5	3.1939	3.1937	3.1937	3.5674
10	12.7211	12.7206	12.7209	12.7642
20	40.9059	40.9056	40.9057	40.89990

**Table. 3** The results of skin friction coefficient in xz-direction  $(Cf_r \operatorname{Re}_x^{1/2})$  for variation of non-dimensional parameters in NM and ANN methods.

Μ	$\beta_{_1}$	$eta_2$	$E_1$	Rd	Ec	Pr	S	Q	Br	$\alpha_{_1}$		$Cf_r \operatorname{Re}_x^{1/2}$	
											NM	ANN	
0.4	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	0.180954	0.175389505	
1	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	0.126905	0.303769159	
1.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	0.412864	0.462084033	
2	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	0.656983	0.638455915	
0.5	0.5	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	0.589509	0.561950011	
0.5	0.7	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	0.828792	0.818177984	
0.5	0.9	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	0.960801	0.970471947	
0.5	1	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	1.011441	1.03990803	
0.5	0.3	0.5	0.5	1	0.05	21	0.3	0.5	1	0.5	0.092991	0.097209999	
0.5	0.3	0.7	0.5	1	0.05	21	0.3	0.5	1	0.5	0.005273	0.021628322	
0.5	0.3	0.9	0.5	1	0.05	21	0.3	0.5	1	0.5	0.10714	0.047722595	
0.5	0.3	1	0.5	1	0.05	21	0.3	0.5	1	0.5	0.15458	0.083779202	
0.5	0.3	0.3	1	1	0.05	21	0.3	0.5	1	0.5	0.503506	0.474899651	
0.5	0.3	0.3	1.5	1	0.05	21	0.3	0.5	1	0.5	0.791431	0.778354012	
0.5	0.3	0.3	2	1	0.05	21	0.3	0.5	1	0.5	1.058272	1.069551658	
0.5	0.3	0.3	2.5	1	0.05	21	0.3	0.5	1	0.5	1.310675	1.361511662	
0.5	0.3	0.3	0.5	1.01	0.05	21	0.3	0.5	1	0.5	0.180955	0.181336731	
0.5	0.3	0.3	0.5	1.02	0.05	21	0.3	0.5	1	0.5	0.180955	0.174620691	
0.5	0.3	0.3	0.5	1.03	0.05	21	0.3	0.5	1	0.5	0.180955	0.173013873	
0.5	0.3	0.3	0.5	1.04	0.05	21	0.3	0.5	1	0.5	0.180952	0.177641111	
0.5	0.3	0.3	0.5	1	0.06	21	0.3	0.5	1	0.5	0.180955	0.062545074	
0.5	0.3	0.3	0.5	1	0.07	21	0.3	0.5	1	0.5	0.180955	0.060015182	
0.5	0.3	0.3	0.5	1	0.075	21	0.3	0.5	1	0.5	0.180955	0.108829085	
0.5	0.3	0.3	0.5	1	0.08	21	0.3	0.5	1	0.5	0.180926	0.195774692	
0.5	0.3	0.3	0.5	1	0.05	22	0.3	0.5	1	0.5	0.180955	0.17040481	
0.5	0.3	0.3	0.5	1	0.05	23	0.3	0.5	1	0.5	0.180955	0.153384096	
0.5	0.3	0.3	0.5	1	0.05	24	0.3	0.5	1	0.5	0.180957	0.142748524	
0.5	0.3	0.3	0.5	1	0.05	25	0.3	0.5	1	0.5	0.180955	0.139546792	
0.5	0.3	0.3	0.5	1	0.05	21	0.4	0.5	1	0.5	0.059617	0.071292267	
0.5	0.3	0.3	0.5	1	0.05	21	0.5	0.5	1	0.5	0.061644	0.065388207	
0.5	0.3	0.3	0.5	1	0.05	21	0.6	0.5	1	0.5	0.182646	0.188357507	
0.5	0.3	0.3	0.5	1	0.05	21	0.7	0.5	1	0.5	0.879077	0.462949872	
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.6	1	0.5	0.180955	0.177856431	
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.7	1	0.5	0.180954	0.173303424	
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.8	1	0.5	0.180955	0.173649336	
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.9	1	0.5	0.180951	0.176309007	
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	2	0.5	0.180954	0.157172958	
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	3	0.5	0.180955	0.140630514	
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	4	0.5	0.180955	0.137576406	
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	5	0.5	0.180956	0.140571371	
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	1	0.180954	0.166158253	
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	1.5	0.180955	0.151442347	
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	2	0.180956	0.148057221	
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	2.5	0.180957	0.152687531	

Μ	$\beta_{_{1}}$	$\beta_2$	$E_1$	Rd	Ec	Pr	S	Q	Br	$\alpha_{_{1}}$	$Cg_r \operatorname{Re}_x^{1/2}$	
											NM	ANN
0.4	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	1.327998	1.340937
1	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	0.662449	0.638885
1.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	0.17261	0.254505
2	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	0.23152	0.223987
0.5	0.5	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	0.141119	0.487026
0.5	0.7	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	0.663203	0.670841
0.5	0.9	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	1.006453	1.007673
0.5	1	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	1.1494	1.155552
0.5	0.3	0.5	0.5	1	0.05	21	0.3	0.5	1	0.5	1.04852	1.055171
0.5	0.3	0.7	0.5	1	0.05	21	0.3	0.5	1	0.5	0.865893	0.872098
0.5	0.3	0.9	0.5	1	0.05	21	0.3	0.5	1	0.5	0.676538	0.683434
0.5	0.3	1	0.5	1	0.05	21	0.3	0.5	1	0.5	0.58649	0.588191
0.5	0.3	0.3	1	1	0.05	21	0.3	0.5	1	0.5	1.586397	1.56276
0.5	0.3	0.3	1.5	1	0.05	21	0.3	0.5	1	0.5	1.900585	1.880991
0.5	0.3	0.3	2	1	0.05	21	0.3	0.5	1	0.5	2.17816	2.168212
0.5	0.3	0.3	2.5	1	0.05	21	0.3	0.5	1	0.5	2.430464	2.417294
0.5	0.3	0.3	0.5	1.01	0.05	21	0.3	0.5	1	0.5	1.212865	1.226756
0.5	0.3	0.3	0.5	1.02	0.05	21	0.3	0.5	1	0.5	1.212864	1.206707
0.5	0.3	0.3	0.5	1.03	0.05	21	0.3	0.5	1	0.5	1.212865	1.189762
0.5	0.3	0.3	0.5	1.04	0.05	21	0.3	0.5	1	0.5	1.212862	1.197756
0.5	0.3	0.3	0.5	1	0.06	21	0.3	0.5	1	0.5	1.212865	1.224325
0.5	0.3	0.3	0.5	1	0.07	21	0.3	0.5	1	0.5	1.212867	1.213953
0.5	0.3	0.3	0.5	1	0.075	21	0.3	0.5	1	0.5	1.204971	1.212355
0.5	0.3	0.3	0.5	1	0.08	21	0.3	0.5	1	0.5	1.204972	1.21708
0.5	0.3	0.3	0.5	1	0.05	22	0.3	0.5	1	0.5	1.212865	1.212476
0.5	0.3	0.3	0.5	1	0.05	23	0.3	0.5	1	0.5	1.212863	1.213684
0.5	0.3	0.3	0.5	1	0.05	24	0.3	0.5	1	0.5	1.212866	1.218493
0.5	0.3	0.3	0.5	1	0.05	25	0.3	0.5	1	0.5	1.212865	1.217806
0.5	0.3	0.3	0.5	1	0.05	21	0.4	0.5	1	0.5	1.021271	1.081952
0.5	0.3	0.3	0.5	1	0.05	21	0.5	0.5	1	0.5	0.828563	0.916587
0.5	0.3	0.3	0.5	1	0.05	21	0.6	0.5	1	0.5	0.634841	0.61765
0.5	0.3	0.3	0.5	1	0.05	21	0.7	0.5	1	0.5	0.256313	0.254465
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.6	1	0.5	1.212865	1.221281
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.7	1	0.5	1.212866	1.209103
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.8	1	0.5	1.212867	1.210062
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.9	1	0.5	1.21286	1.215866
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	2	0.5	1.212864	1.207685
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	3	0.5	1.212865	1.210535
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	4	0.5	1.212866	1.207033

**Table. 4** The results of skin friction coefficient in yz-direction  $(Cg_r \operatorname{Re}_x^{1/2})$  for variation of non-dimensional parameters in NM and ANN methods.

0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	5	0.5	1.212866	1.213101
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	1	1.212864	1.229174
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	1.5	1.212865	1.218506
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	2	1.2128656	1.217304
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	2.5	1.212868	1.226123

**Table. 5** The results of heat transfer coefficient (Nusselt number  $Nu_x \operatorname{Re}_x^{-1/2}$ ) for variation of non-dimensional parameters in NM and ANN methods.

M	$\beta_{_1}$	$\beta_{2}$	$E_1$	Rd	Ec	Pr	S	Q	B	$r \alpha_1$	$Nu_x \operatorname{Re}_x^{-1/2}$	2
											NM	ANN
0.4	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	17.000741	16.82814
1	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	16.567447	16.48499
1.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	16.092525	16.08554
2	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	15.60204	15.59453
0.5	0.5	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	16.462047	16.34181
0.5	0.7	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	16.083963	16.03002
0.5	0.9	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	15.889186	15.85824
0.5	1	0.3	0.5	1	0.05	21	0.3	0.5	1	0.5	15.798502	15.76673
0.5	0.3	0.5	0.5	1	0.05	21	0.3	0.5	1	0.5	16.591513	16.56418
0.5	0.3	0.7	0.5	1	0.05	21	0.3	0.5	1	0.5	16.597923	16.53073
0.5	0.3	0.9	0.5	1	0.05	21	0.3	0.5	1	0.5	16.590622	16.59721
0.5	0.3	1	0.5	1	0.05	21	0.3	0.5	1	0.5	16.584462	16.57361
0.5	0.3	0.3	1	1	0.05	21	0.3	0.5	1	0.5	16.348064	16.33492
0.5	0.3	0.3	1.5	1	0.05	21	0.3	0.5	1	0.5	15.860596	15.79266
0.5	0.3	0.3	2	1	0.05	21	0.3	0.5	1	0.5	15.17239	15.1144
0.5	0.3	0.3	2.5	1	0.05	21	0.3	0.5	1	0.5	14.308991	14.30859
0.5	0.3	0.3	0.5	1.01	0.05	21	0.3	0.5	1	0.5	16.634018	16.71902
0.5	0.3	0.3	0.5	1.02	0.05	21	0.3	0.5	1	0.5	16.700332	16.69104
0.5	0.3	0.3	0.5	1.03	0.05	21	0.3	0.5	1	0.5	16.766395	16.72045
0.5	0.3	0.3	0.5	1.04	0.05	21	0.3	0.5	1	0.5	16.832208	16.81933
0.5	0.3	0.3	0.5	1	0.06	21	0.3	0.5	1	0.5	16.350909	16.41846
0.5	0.3	0.3	0.5	1	0.07	21	0.3	0.5	1	0.5	16.133422	16.13728
0.5	0.3	0.3	0.5	1	0.075	21	0.3	0.5	1	0.5	16.024311	16.01738
0.5	0.3	0.3	0.5	1	0.08	21	0.3	0.5	1	0.5	15.914968	15.9082
0.5	0.3	0.3	0.5	1	0.05	22	0.3	0.5	1	0.5	16.947166	16.94725
0.5	0.3	0.3	0.5	1	0.05	23	0.3	0.5	1	0.5	17.317468	17.17922
0.5	0.3	0.3	0.5	1	0.05	24	0.3	0.5	1	0.5	17.678965	17.58596
0.5	0.3	0.3	0.5	1	0.05	25	0.3	0.5	1	0.5	18.032213	18.03619
0.5	0.3	0.3	0.5	1	0.05	21	0.4	0.5	1	0.5	16.725507	16.71665
0.5	0.3	0.3	0.5	1	0.05	21	0.5	0.5	1	0.5	16.863043	16.69781
0.5	0.3	0.3	0.5	1	0.05	21	0.6	0.5	1	0.5	16.980051	16.82854
0.5	0.3	0.3	0.5	1	0.05	21	0.7	0.5	1	0.5	17.075629	17.06855
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.6	1	0.5	16.53894	16.63236
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.7	1	0.5	16.510421	16.50309

0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.8	1	0.5	16.481884	16.43332
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.9	1	0.5	16.453333	16.44709
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	2	0.5	16.567447	16.57789
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	3	0.5	16.567447	16.50601
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	4	0.5	16.567447	16.56003
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	5	0.5	16.567447	16.54298
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	1	16.567447	16.82961
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	1.5	16.567447	16.74716
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	2	16.567447	16.56055
0.5	0.3	0.3	0.5	1	0.05	21	0.3	0.5	1	2.5	16.567447	16.35167

# **Biographies**

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