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Optimum recovery time for cyclic compression tests on bovine brain tissue

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KEYWORDS Recovery time; Preconditioning effect; Strain history; Brain tissue modeling, Bovine brain tissue. Abstract. In conducting mechanical tests on the brain tissue, it is preferred to perform multiple tests on the same sample. In this study, we investigated the behavior of the bovine brain tissue in repeated compression tests with 6 recovery periods (namely, 10, 60, 120, 180, 240, and 300 s). Compression tests were performed on cylindrical samples with average diameter and height of 18.0 mm and 15.0 mm, respectively. Two testing protocols were employed; the first one comprised experiments with 5, 25, and 125 mm/min loading speeds up to 33% strain and the second one consisted of tests with 25 and 125 mm/min loading speeds up to 17% strain. Each experiment was conducted in two cycles separated by a specific recovery period. Stress-strain data from the first and second cycles were compared using 3 criteria, namely Normalized Root-Mean-Square Error (NRMSE), coefficient of variation (R^2), and Effective Height Ratio (EHR). The analysis suggested that the optimum recovery periods for the first and second protocols were 120 s and 180 s, respectively. Moreover, differences between the first and second cycles in medium- and high-speed tests were found to be smaller than those in the low-speed experiments.

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1. Introduction

Mechanical modeling has widely been used to study the behavior of human brain in different circumstances such as Traumatic Brain Injury (TBI) [1-4] and tumor growth [5,6]. Material properties of brain tissue critically affect the accuracy of simulations. Despite numerous studies aiming at characterizing mechanical properties of the brain tissue, there is still considerable variation between results (for more information, see [7,8]). Part of the discrepancy between studies can be ascribed to the absence of a standardized testing

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protocol. Generally, mechanical testing protocols for the brain tissue can be classified into two groups: First, experiments in which only one loading cycle is performed on each sample [9-13]; and second, studies that perform multiple tests (of one or various types) on each sample to eliminate inter-species variation and/or to assess the effect of preconditioning on the brain tissue [14-18]. The second group can be divided into preconditioned and non-preconditioned protocols. Preconditioning cycles are often performed on samples in order to obtain statistically even data and improve reproducibility [19]. However, there is still controversy over the validity of preconditioned data for some circumstances such as TBI [20]. In non-preconditioned protocols, there is a recovery period between loading cycles, which allows the tissue to recover from the specimen "memory;" this effect results from tissue viscoelasticity and prevents the sample from resetting to its reference state. Using non-preconditioned protocols with sufficient recovery period, the inter-species variation would be eliminated. Moreover, negative effects caused by sample preparation and handling would be reduced. The preconditioning effect and recovery period of various tissue types have been investigated (aortic valve tissue [21], tendons and collagen fibers [22,23], and skin [24-26]). In contrast, there are only a small number of studies investigating the recovery time of the brain tissue. Prange and Margulies [27] used 60 s recovery time and showed that the first and final long-term shear moduli for 5 percent shear test were similar. Gefen and Margulies [20] stated that brain tissue did not fully recover in 45 s. However, their study did not specify the time in which recovery was achieved. Dommelen et al. [16] investigated the minimum recovery time for both gray and white matter. Indentation tests with spherical indenter 2 mm in diameter were performed. The recovery time of 50 s was found to be adequate for both white and gray matter. However, no details about data comparison, criteria, and the number of tests were reported. Prevost and Balakrishnan [28] found that brain samples recovered their original response after 2 h rehydration period. In another study, Prevost et al. [29] performed cyclic indentation tests in-vivo, in-situ, and in-vitro on porcine brain tissue. They suggested that tissue could recover from preconditioning effect when allowed to rest for 2 minutes. Nonetheless, the criteria used in their study were only peak forces and the heights of initial and final cycles. Hence, the differences between data points of the initial and final states were ignored. Most recently, Budday et al. [14] observed that the brain tissue would show the same stress-strain pattern after 60 min recovery period. However, their finding is just an observation and cannot be used as a reference for recovery time. The objective of this study is to assess the optimum recovery time for the bovine brain tissue. Furthermore, we aim to study the variation of the recovery time concerning strain level and rate.

2. Materials and methods

2.1. Sample preparation

Fresh bovine brains were obtained from a local slaughterhouse. The reason behind choosing bovine tissue was availability and lowering of post-mortem hours. Six intact brains were placed in ice-cooled Phosphate Buffered Saline (PBS) in order to prevent dehydration and degeneration. Brains were first split into the right and left hemispheres from sagittal plane. A steel pipe with the inner diameter of 22 mm was used for sample acquisition. Figure 1 shows the cutting tool. The samples were excised from all sites of the brain to cover a wide range of tissue properties. Thereafter, each cylindrical specimen was cut to the height of 15 mm.



Figure 1. Cylindrical cutting tool. A stainless steel tube with inner and outer diameters of 22 mm and 25 mm was sharpened at one end. Samples were excised by rotational movement of this tube.

Despite using a cutting tool with fixed dimensions, specimen diameter ranged between 17 to 21.5 with a mean diameter of 18.0 ± 1.2 mm. The discrepancy between the cutting tool and specimen diameter was mainly because of the tension exerted on the surface of the tissue during the process of sample excision. This tensile force induced stretch in the tissue surface. Immediately after excision, surface area was reduced to its original state. Certain features were defined to distinguish high-quality samples form low-quality ones:

- Arachnoid membrane should be intact on the bottom surface of the sample (cerebral cortex). This criterion assures that sulci will remain unchanged during the test and will not cause a sudden change in dimensions of the specimen;
- Top and bottom surfaces of the sample (i.e., ventricle and cerebral cortices, respectively) should be flat and even. The concave surface would result in unfavorable adhesion to plates. Moreover, uneven surface will increase the possibility of buckling. A sample with common flaws is depicted in Figure 2.

Overall, 40 samples were obtained from 6 brains. Compression tests proceeded by measuring sample diameter individually. Measurements were done at the top, middle, and bottom of each sample and average diameter was used for further calculations. Generally, the diameter of the top and bottom surfaces varied by approximately 3-4 mm. Hence, samples were in the form of a truncated cone instead of a cylinder. Unconfined boundary condition was achieved by utilization of lubricant on both upper and lower plates.



Figure 2. Common defects of a low-quality sample. Sulci opening causes dramatic changes in diameter and height. Uneven surface leads to asymmetric force distribution, which may in turn increase the possibility of buckling.



Figure 3. Sample placement in the testing machine. Upper and lower plates of the testing machine were lubricated before the experiment to provide unconfined boundary condition.

This step was especially important for preventing the barreling effect. Finally, each specimen was taken out of ice-cooled PBS solution and placed between plates as shown in Figure 3.

2.2. Experimental set-up

The main apparatus for conducting tests was a Zwick/Roell Z050 universal testing machine. It was equipped with a servomotor, which could provide the loading speed of 0.001 to 2000 mm/min. A 5 kgf load cell was mounted on the machine, allowing the force measurement between 0.001 to 50 N. The Zwick/Roell Windows-based software had the capacity to conduct programmed tests. Hence, there was no need for manual set-up for every sample and the results were improved by reducing testing time.

2.3. Test procedure

Two testing protocols were organized to cover 6 recovery times at 2 strain levels. Protocol 1 consisted of



Figure 4. Schematic of the testing protocol. Recovery periods included 10, 60, 120, 180, 240, and 300 s.

tests with loading speeds of 5, 25, and 125 mm/min (0.005, 0.025, and 0.125/s strain rates, respectively).Testing speeds for Protocol 2 were 25 and 125 mm/min. The separation between parallel plates of the testing machine was fixed to 15 mm, and it was set up to have displacements of 5 and 2.5 mm for Protocols 1 and 2 (33% and 17% strains), respectively. However, the height of samples was generally slightly less than Therefore, test results deviated from the 15 mm. nominal strain level. Schematic of the testing protocols is illustrated in Figure 4. Recovery periods were 10, 60, 120, 240, and 300 s. By the time the test started, the lower plate had moved up with constant speed and compressed the tissue up to the pre-set displacement. Immediately, it began coming down with the same speed. After the recovery period was passed, an identical cycle started automatically.

From the 40 samples excised from brains, 10 samples were recognized as low-quality. Furthermore, 2 samples failed during the tests and were eliminated. All tests were conducted in the room temperature ($\sim 24^{\circ}$ C) and within the 28 h postmortem.

2.4. Data analysis

To find the optimum recovery time, differences between the first and second cycles should be assessed. Comparison between the two cycles was performed using the following criteria:

• Effective Height Ratio (EHR):

$$EHR = \frac{L^{(2)}}{L^{(1)}} \times 100.$$
(1)

 $L^{(i)}$ stands for the length of the *i*th cycle. The length of each cycle is measured by reading the first force having the order of mN. This parameter demonstrates the amount of residual deformation. Higher EHR values indicate that the tissue has recovered its reference height. Moreover, residual deformation values were calculated for more details; • Normalized Root-Mean-Squared Error (NRMSE):

$$RMSE = \sqrt{\frac{1}{n} \sum_{i=1}^{n} \left(\sigma_i^{(1)} - \sigma_i^{(2)}\right)^2},$$
 (2)

$$NRMSE = 100 \times \frac{\text{RMSE}}{\sigma_{\text{max}}^{(1)} - \sigma_{\text{min}}^{(1)}}.$$
 (3)

Symbols $\sigma^{(k)}$ and *n* represent the normal stress on the *k*th cycle and number of data points, respectively. Normalizing RMSE guarantees that errors are independent of stress range. This process is important since samples are obtained from various parts of the brain and have different maximum stress values.

• Coefficient of determination (R^2) :

$$R^{2} = 100 \times \left(1 - \frac{\sum_{i=1}^{n} \left(\sigma_{i}^{(1)} - \sigma_{i}^{(2)}\right)^{2}}{\sum_{i=1}^{n} \left(\sigma_{i}^{(1)} - \bar{\sigma}\right)^{2}}\right).$$
 (4)

The $\bar{\sigma}$ and $\sigma^{(k)}$ signs stand for the mean stress value of the first cycle and normal stress of the *k*th cycle, respectively.

Unlike the criteria used by Prevost et al. [29], the aforementioned criteria assess not only the final-state differences (such as EHR), but also similarities between all data points. Hence, the comparison between the first and second cycles will be comprehensive.

3. Results

In all tests, variation of peak stress values between different samples is noticeable. The stress-strain curves for experiments with medium loading speed (i.e., 25 mm/min) from Protocols 1 and 2 are depicted in Figures 5 and 6, respectively. As a result of the presence of residual strain, the second cycle tended to reach strain levels smaller than that of the first cycle. Hence, NRMSE and R^2 were computed up to the maximum strain of the second cycle. Tests with the speed of 5 mm/min (Protocol 1) were challenging due to their longer testing time. Samples having 60 and 180 s recovery periods from Protocol 1 demonstrated signs of sulci opening and slip. Therefore, their test data was excluded. High strain level experiments (Protocol 1) tended to have smaller EHR values than low strain tests (Protocol 2). Moreover, a significant increase in the EHR was observed as the loading speed increased from the speed of 5 to 25 mm/min in Protocol 1 (Figure 7(a)). In contrast, the EHR values in Protocol 2 were recognized to have negligible variation (Figure 7(b)). The values of residual deformation are shown in Table 1 in more details.

NRMSE variation for Protocol 1 is illustrated in Figure 8(a). Generally, testing speed had a reverse relationship with the amount of normalized error. This result implies that low-speed tests need more time to recover. NRMSE reached its minimum after 180 s for Protocol 1. The response of tissue to different



Figure 5. Stress-strain curves for the loading speed of 25 mm/min in Protocol 1. Plot titles indicate the recovery period. Both curves for the first and second cycles are adjusted to begin from 0% strain level. Hence, the second cycle is compressed to a lower level of strain due to the presence of residual strain. Despite the closeness of the stress values for the first and second cycles in the initial and final parts of the curve, they are mainly separated in middle parts.

2206



Figure 6. Stress-strain curves for the loading speed of 25 mm/min belonging to Protocol 2. Plot titles indicate the recovery period. Curves for the first and second cycles are close to each other compared with those in Protocol 1.



Figure 7. EHR variation for: (a) Protocol 1 and (b) Protocol 2. Generally, the amount of EHR increases with the rise of the loading speed from 5 to 25 mm/min for Protocol 1. Residual strain for Protocol 2 appears to be slightly lower than that for Protocol 1.

recovery times in Protocol 2 regarding NRMSE is shown in Figure 8(b). It can be considered as upward concave with its minimum at 120 s. Long recovery periods appeared to paradoxically increase error for



Figure 8. NRMSE values for: (a) Protocol 1 and (b) Protocol 2. Overall, the amount of error decreases as the testing speed increases from 5 to 25 mm/min for Protocol 1. The minimum error values occur at 120 and 180 s recovery times for Protocols 1 and 2, respectively.

both protocols. This phenomenon implies that long recovery periods outside PBS solution would have a significantly negative effect on the tissue behavior.

 R^2 , on the other band, appeared to demonstrate

Table 1. Residual deformation values for Protocols 1 and 2. The first reading force in the range of 1-4 mN was stipulated as the start point and the corresponding displacement value was used to calculate the effective height of the sample for each cycle. The mean value demonstrated decrease in residual deformation with the rise of the test speed. Moreover, Protocol 2 had smaller values than Protocol 1.

Residual deformation (mm)								
		RP [*] (s)						
	Speed $\frac{mm}{min}$	10	60	120	180	240	300	$\rm Mean\pmStd^{**}$
Protocol 1	5	0.84	N/A	0.50	N/A	0.29	0.92	0.63 ± 0.29
	25	0.32	0.36	0.10	0.13	0.24	-0.01	0.19 ± 0.14
	125	0.19	0.12	0.22	0.10	0.01	0.11	0.12 ± 0.07
Protocol 2	25	0.14	0.04	0.03	0.07	0.10	0.14	0.08 ± 0.04
	125	0.07	0.05	0.06	0.13	0.00	0.05	0.06 ± 0.04

*: Recovery period; **: Standard deviation.



Figure 9. R^2 values for: (a) Protocol 1 and (b) Protocol 2.

an upward convex curve with its minimum at 180 s for Protocol 1 (Figure 9(a)). Nonetheless, R^2 curve for Protocol 2 reached its maximum after 120 s recovery period (Figure 9(b)).

4. Discussion

2208

This study investigates preconditioning effect and the impact of recovery time of compression tests on the bovine brain tissue. Two testing protocols were proposed to cover several recovery periods, strain rates, and strain levels. Primary interests of this study were, first, determination of the recovery time enough to assure negligibility of the "memory" effect, yet small enough not to affect test results negatively by elongating the experiment; and second, investigating the dependency of recovery time on the strain rate and strain level. The experimental results of this study indicated that for different testing conditions, various recovery periods should be implemented. However, further investigations into this subject are required to make the testing protocols converge, aiming to study mechanical properties of the brain tissue. The current study has some limitations that can be categorized as follows:

- 1. Testing protocols included only one mode of deformation (unconfined uniaxial compression);
- 2. Samples were a combination of white and gray matter. Consequently, due to the weak connection between the white and gray matter of the brain, the possible separation of these two tissue types under compression might have caused discrepancies in the test data [30]. Furthermore, samples were selected randomly from different sites of the brain. Hence, results of this study can be used as an average value for the recovery period;
- 3. Due to the presence of sulci, measurements may have been affected by the local opening of sulci (samples were examined before the test to avoid flaws. Moreover, test data with patterns indicating sulci defect were excluded);
- 4. Local adhesion of the top surface of the sample (which was white matter) might have changed the response of tissue during unloading (top and bottom plates were continuously lubricated to reduce the adhesion);
- 5. Uneven top surface of the sample may have disturbed data acquisition (top face was smoothened by a surgical flap to avoid concave/rough surface).

Brain samples were observed to undergo mechanical softening after the first cycle (see Figures 5 and 6). This behavior has been reported in the literature [14,20]. Moreover, it can be observed that even though the initial and final parts of the stressstrain curves for the first and second cycles are close to one another, they are separated in middle parts. Hence, the criteria that consider only the initial and final differences of the two cycles may result in misleading interpretation of the suitable recovery period. Therefore, the criteria based on all data points are recommended.

According to the results of this study, residual deformation decreases as the testing speed increases (see Table 1). Prevost et al. [29] reported the same trend for 2 min recovery period with in-vitro experiments. Moreover, residual deformation values between the two studies are close to each other. EHR values for Protocol 1 demonstrate high dependency on strain rate. Low strain rate test (5 mm/min) appeared to have significantly smaller values of EHR than mediumand high-speed tests did (see Figure 7(a) and Table 1). We surmise that this behavior can be ascribed to the diffusion of interstitial fluid of the samples. The longer the tissue is deformed under compression, the more fluid flows outside the sample. This process may make the sample unrecoverable. Hence, an additional step should be included in the recovery process: samples should be placed in an appropriate solution to absorb the fluid [28].

Generally, the mean values of NRMSE and R^2 for Protocol 1 suggest that the tissue can be considered recovered after 180 s (Figures 8(a) and 9(a)) with mean NRMSE and R^2 of 2.5% and 99.0%, respectively. It should be noted that we will obtain the same results for recovery time with elimination of data from experiments with loading speed of 5 mm/min. For Protocol 2, 120 s is suggested as recovery period with mean NRMSE and R^2 of 1.5% and 99.5%, respectively (Figures 8(b) and 9(b)). This finding is in contrast with the suggestion of Dommelen et al. [16]. They stated that reproducibility was achieved with 50 s recovery period. They used local indentation with the indenter diameter of 2 mm. Based on interstitial fluid diffusion theory [28], we believe that the results of local indentation cannot be applied to finite deformation compressive tests. Local indentation leads to a small amount of fluid diffusion, and the volume of fluid that exits the sample is negligible and it quickly recovers. Moreover, due to the absence of data analysis, concrete discussion cannot be made. The results of this study suggest that the difference of NRMSE and R^2 between the first and second cycles decreases with the enhancement of testing speed, while Prevost et al. [29] stated the opposite. NRMSE and R^2 values indicate that long recovery periods out of physiological fluid negatively affect the recovery process. As recovery time elongates, samples start to creep under their own weight. Moreover, inner parts of the tissue may be dehydrated, even though the surface of the tissue is

hydrated during the recovery period. Altogether, we suggest 2 min recovery time for low-strain compression ($\sim 17\%$) and 3 min for high-strain compression ($\sim 33\%$).

5. Conclusion

This study investigated the recovery period and preconditioning effect of the brain tissue. Currently, there are few studies with the primary goal in this subject. To initiate a comprehensive study, two protocols were proposed to assess the recovery time in various conditions. Three loading speeds (namely 5, 25, and 125 mm/min), 2 levels of strain (namely 30 and 17%), and 6 recovery times (namely 10, 60, 120, 180, 240, and 300 s) were employed. The results of this study presented optimum recovery time for each strain level. We suggested 2 and 3 min recovery times for low- and high-strain levels $(\sim 17\%$ and 33% respectively). The suggested values were valid for the domain of protocols used in this study. Based on the trends observed in this study, we predicted that quasi-static tests might need additional treatment (e.g., placing the sample in PBS after the first cycle) for recovery. However, more investigations should be carried out to assess the recovery time for different test speeds and different regions/orientations of the brain tissue. Assessment of recovery time for white and gray matter separately would be of great importance. We believe that investigating various factors affecting testing conditions such as preconditioning, postmortem hours, and temperature would decrease the variations between the results of testing protocols. Therefore, a standard testing procedure can be created. Subsequently, consensus of the results on brain tissue properties may be achieved.

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References

- Cloots, R.J.H., Van Dommelen, J.A.W., Kleiven, S., and Geers, M.G.D. "Multi-scale mechanics of traumatic brain injury: Predicting axonal strains from head loads", *Biomech. Model. Mechanobiol.*, 12(1), pp. 137-150 (2013).
- Friedman, R., Epstein, Y., and Gefen, A., Traumatic Brain Injury in the Military: Biomechanics and Finite Element Modelling BT - The Mechanobiology and Mechanophysiology of Military-Related Injuries, A. Gefen and Y. Epstein, Eds. Cham: Springer International Publishing, pp. 209-233 (2016).
- Sahoo, D., Deck, C., Yoganandan, N., and Willinger, R. "Development of skull fracture criterion based on real-world head trauma simulations using finite ele-

ment head model", J. Mech. Behav. Biomed. Mater., 57, pp. 24-41 (2016).

- Clark, J.M., Hoshizaki, T.B., and Gilchrist, M.D. "Assessing women's lacrosse head impacts using finite element modelling", J. Mech. Behav. Biomed. Mater., 80, pp. 20-26 (2018).
- Kansal, A.R., Torquato, S., Harsh IV, G.R., Chiocca, E.A., and Deisboeck, T.S. "Simulated brain tumor growth dynamics using a three-dimensional cellular automaton", J. Theor. Biol., 203(4), pp. 367-382 (2000).
- Wong, K.C.L., Summers, R.M., Kebebew, E., and Yao, J. "Tumor growth prediction with reaction-diffusion and hyperelastic biomechanical model by physiological data fusion", *Med. Image Anal.*, 25(1), pp. 72-85 (2015).
- Hrapko, M., Van Dommelen, J.A., Peters, G.W., and Wismans, J.S. "The influence of test conditions on characterization of the mechanical properties of brain tissue", J. Biomech. Eng., 130(3), p. 31003 (2008).
- Cheng, S., Clarke, E.C., and Bilston, L.E. "Rheological properties of the tissues of the central nervous system: A review", *Med. Eng. Phys.*, **30**(10), pp. 1318-1337 (Dec. 2008).
- Miller, K. and Chinzei, K. "Constitutive modelling of brain tissue: Experiment and theory", J. Biomech., 30(11-12), pp. 1115-1121 (1997).
- Miller, K. and Chinzei, K. "Mechanical properties of brain tissue in tension", J. Biomech., 35(4), pp. 483-490 (2002).
- Jin, X., Zhu, F., Mao, H., Shen, M., and Yang, K.H. "A comprehensive experimental study on material properties of human brain tissue", J. Biomech., 46(16), pp. 2795-2801 (2013).
- Budday, S., Nay, R., De Rooij, R., et al. "Mechanical properties of gray and white matter brain tissue by indentation", J. Mech. Behav. Biomed. Mater., 46, pp. 318-330 (2015).
- Rashid, B., Destrade, M., and Gilchrist, M.D. "Mechanical characterization of brain tissue in tension at dynamic strain rates", J. Mech. Behav. Biomed. Mater., 33(1), pp. 43-54 (2014).
- Budday, S., Sommer, G., Birkl, C., et al. "Mechanical characterization of human brain tissue", Acta Biomater., 48, pp. 319-340 (2017).
- Bilston, L.E., Liu, Z., and Phan-Thien, N. "Linear viscoelastic properties of bovine brain tissue in shear", *Biorheology*, **34**(6), pp. 377-385 (1997).

- Van Dommelen, J.A.W., Van Der Sande, T.P.J., Hrapko, M., and Peters, G.W.M. "Mechanical properties of brain tissue by indentation: Interregional variation", *J. Mech. Behav. Biomed. Mater.*, 3(2), pp. 158-166 (2010).
- Destrade, M., Gilchrist, M.D., Murphy, J.G., Rashid, B., and Saccomandi, G. "Extreme softness of brain matter in simple shear", *Int. J. Non. Linear. Mech.*, 75, pp. 54-58 (2015).
- Labus, K.M. and Puttlitz, C.M. "Viscoelasticity of brain corpus callosum in biaxial tension", J. Mech. Phys. Solids, 96, pp. 591-604 (2016).
- Fung, Y.-C., Biomechanics: Mechanical Properties of Living Tissues, 2nd Ed. New York, NY: Springer New York (1993).
- Gefen, A. and Margulies, S.S. "Are in vivo and in situ brain tissues mechanically similar?", J. Biomech., 37(9), pp. 1339-1352 (2004).
- Carew, E.O., Barber, J.E., and Vesely, I. "Role of preconditioning and recovery time in repeated testing of aortic valve tissues: Validation through quasilinear viscoelastic theory", Ann. Biomed. Eng., 28(9), pp. 1093-1100 (Sep. 2000).
- Hubbard, R.P. and Chun, K. "Mechanical responses of tendons to repeated extensions and wait periods", J. Biomech. Eng., 110, pp. 11-19 (Feb. 1988).
- Sverdlik, A. and Lanir, Y. "Time-dependent mechanical behavior of sheep digital tendons, including the effects of preconditioning", J. Biomech. Eng., 124(1), pp. 78-84 (2002).
- Lanir, Y. and Fung, Y.C. "Two-dimensional mechanical properties of rabbit skin-II. Experimental results", J. Biomech., 7(2), pp. 171-182 (1974).
- Vogel, H.G. and Denkel, K. "In Vivo recovery of mechanical properties in rat skin after repeated strain", *Arch. Dermatol. Res.*, 277(6), pp. 484-488 (1985).
- Remache, D., Caliez, M., Gratton, M., and Dos Santos, S. "The effects of cyclic tensile and stressrelaxation tests on porcine skin", J. Mech. Behav. Biomed. Mater., 77, pp. 242-249 (2018).
- Prange, M.T. and Margulies, S.S. "Regional, directional, and age-dependent properties of the brain undergoing large deformation", J. Biomech. Eng., 124(2), p. 244 (2002).
- Prevost, T.P., Balakrishnan, A., Suresh, S., and Socrate, S. "Biomechanics of brain tissue", Acta Biomater., 7(1), pp. 83-95 (2011).
- Prevost, T.P., Jin, G., De Moya, M.A., Alam, H.B., Suresh, S., and Socrate, S. "Dynamic mechanical response of brain tissue in indentation in vivo, in situ and in vitro", *Acta Biomater.*, 7(12), pp. 4090-4101 (2011).
- Cheng, S. and Bilston, L.E. "Unconfined compression of white matter", J. Biomech., 40(1), pp. 117-124 (2007).

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