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Profile and wavefront optimization by metaheuristic algorithms for efficient finite element analysis

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KEYWORDS

Profile and wavefront reduction; Ordering; Colliding Bodies Optimization (CBO); Enhanced Colliding Bodies Optimization (ECBO); Tug of War Optimization (TWO); Vibrating Particles System (VPS). Abstract. To efficiently solve the equations that arise from finite element analysis, the stiffness matrix of a model should be structured. This can be achieved by reducing the profile or wavefront of the corresponding graph matrix of a structure depending on whether the skyline or frontal method is used. One of the efficient methods for achieving this goal is the method of King, extended by Sloan. In this paper, the coefficients of the priority function utilized in the generalized Sloan's method are optimized using the recently developed metaheuristic algorithm, called vibrating particles system. The results are compared with those of other metaheuristic algorithms consisting of the particle swarm optimization, colliding bodies optimization, enhanced colliding bodies optimization, and tug of war optimization. These metaheuristics are used for optimum nodal numbering of the graph models of the finite element meshes to reduce the profile and wavefront of the corresponding sparse matrices. The comparison of the results of the metaheuristic algorithms and those of the King and Sloan demonstrates the efficiency of the new metaheuristic algorithm utilized for profile and wavefront optimization.

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1. Introduction

The solution to the sparse systems of simultaneous equations comprises every main element of many problems in structural engineering. Such linear algebraic equations appear in the form of Ax = b arising from matrix structural analysis and finite element methods. These types of equations often involve a positive definite, symmetric, and sparse matrix coefficient A. For large structures, a great deal of computational time and memory is usually dedicated to finding a solution to these equations. Therefore, some suitable specific patterns for the coefficients of the corresponding equations have been provided such as banded form, profile form, and blocked form. These patterns can often be obtained by the nodal ordering of the corresponding models.

In the Finite-Element Model (FEM) analysis, when the nodes have one degree of freedom, performing nodal ordering is equivalent to reordering the equations. In a more general problem, for each node with m degree of freedom, there are m coupled equations produced for each node. In such cases, re-sequencing is usually performed on the nodal numbering of the graph models to reduce the bandwidth, profile or wavefront, because the size of these problems is mfold smaller than that with m degree of freedom numbering. In this article, the mathematical model

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of the FEM is considered as an element clique graph, and nodal ordering is carried out to reduce the profile and wavefront of the corresponding matrices [1-3].

For nodal numbering in the solution of sparse systems, the following rule can be used: permuting rows and columns of a matrix by the proper renumbering of the nodes of the corresponding graph. Two important parameters in nodal ordering are profile and wavefront optimization. In fact, for sparse matrices, the size of the problem can be measured by the profile or wavefront of such matrices. These problems produced considerable interest in the past because of its practical relevance for a significant range of global optimization applications. Since the problem of nodal numbering is NP-Complete [4], many approximate approaches and heuristics have been proposed, examples of which can be found in Gibbs et al. [5], Cuthill and McKee [6], Kaveh [1], Bernardes and Oliveira [7], King [8], Kaveh and Behzadi [9], Kaveh and Roosta [10], and Koohestani and Poli [11].

Recently generated optimization methods consist of metaheuristic algorithms that solve complex problems. These techniques explore a feasible region based on both randomization and some specific rules through a group of search agents. The rules are usually inspired by the laws of natural phenomena [12].

As a recently developed type of metaheuristic approach, Colliding Bodies Optimization (CBO) was introduced and employed in structural problems by Kaveh and Mahdavi [13]. CBO is a multi-agent method and is inspired by a one-dimensional collision between two agents. Each object is considered as a body with a specific mass and a velocity. A collision occurs between a pair of bodies, and the new positions of the colliding bodies are updated based on the laws of collision. The enhanced colliding bodies optimization introduced by Kaveh and Ilchi Ghazaan [14] employs memory in order to save the best-so-far position to improve the performance of CBO without increasing the computer execution time. This algorithm also utilizes a mechanism to escape local optima. A multiagent metaheuristic algorithm, called tug of war optimization, was introduced by Kaveh and Zolghadr [15]. This technique models each candidate solution as a team engaged in a series of tug of war competitions. The weight of the teams is determined based on the quality of the corresponding solutions, and the value of pulling force that a team can exert on the rope is assumed to be proportional to its weight. VPS is a population-based optimization algorithm, which is inspired by a free vibration of a single degree of freedom systems with viscous damping, as was introduced by Kaveh and Ilchi Ghazaan [16]. In this method, the solution candidates are considered as agents that gradually approach their equilibrium positions. In order to ensure a proper balance between exploration and exploitation, equilibrium positions are attained from the current population and the best historical position.

The rest of this paper is organized as follows: in Section 2, some definitions of graph theory, profile, and wavefront are presented. CBO, ECBO, TWO, and VPS algorithms are briefly stated in Section 3. In order to show the performance of these methods in reducing the profile and wavefront of the stiffness matrix, eight examples are presented in Section 4. The last section concludes the present study.

2. Problem definition

2.1. Definitions from the theory of graphs

Let G(N, M) be a graph with a set of members M(|M| = m) and a set of nodes N(|N| = n) together with a relation of incidence. The *degree* of a node is the number of members, which are incidental to that node; 1-weighted degree of a node is defined as the sum of the degrees of its adjacent nodes. A spanning tree is a tree containing all the nodes of S. The Shortest Route Tree (SRT_{n_0}) rooted in a considered node (starting node), n_0 , is a spanning tree where the distance between every node n_i of S and n_0 is minimum and where the *distance* between the two nodes is taken to be the number of members in the shortest path between these nodes. A contour $C_k^{n_0}$ contains all the nodes with equal distance k from node n_0 . The number of contours of an SRT_{n_0} is known as its *depth*, denoted by $d(\operatorname{SRT}_{n_0})$, and the highest number of nodes in a contour shows the width of SRT_{n_0} . A label As of G assigns a set of integers $\{1, 2, 3, \dots, n\}$ to the nodes of graph G. As(i) is the label or the integer assigned to node i, and each node has a different label [2].

The profile of an $N \times N$ matrix related to graph G, for the assignment process by As(i), is defined as follows:

$$P_{As} = \sum_{i=1}^{N} b_i,\tag{1}$$

where the row bandwidth, b_i , for row i is defined as the number of inclusive entries from the first nonzero element in the row to the (i + 1)th entry for this assignment. The efficiency of the given ordering for the profile solution scheme corresponds to the number of active equations during each step of the factorization process. Formally, row j is defined to be active during elimination of column i if $j \ge i$, and there exists $a_{ik} = 0$ with $k \le i$. Hence, in the *i*th stage of the factorization, the number of active equations is the number of rows of profile that intersect in column i, where the already eliminated rows are ignored. Let f_i denote the number of equations that are active during the elimination of variable x_i . It follows from the symmetric structures of the matrix that:

$$P_{As} = \sum_{i=1}^{N} f_i = \sum_{i=1}^{N} b_i, \qquad (2)$$

where f_i is the frontwidth or wavefront. Assuming that N and the average value of f_i are considerably large, it can be shown that a complete profile or front factorization needs approximately $O(NF_{rms}^2)$ operations, where F_{rms} is the root-mean square frontwidth, which is defined as follows:

$$F_{rms} = \left[\frac{1}{N}\sum_{i=1}^{N}f_{i}^{2}\right]^{0.5}.$$
(3)

For the purpose of obtaining an optimal nodal ordering in the profile and frontwidth reduction problems, the set of integers $\{1, 2, 3, \dots, n\}$ should be assigned to the nodes of G using a priority function, and the coefficients of the priority functions are obtained using PSO, CBO, ECBO, TWO, and VPS algorithms.

2.2. An algorithm based on priority queue for profile and wavefront reduction

The nodal numbering in a priority queue is carried out through the assignment of status based on the numbering approach of King [8]. King's method was generalized by Sloan [17] by introducing a priority queue that controls the order to be followed in the numbering of the nodes. This algorithm comprises two phases:

Phase 1: Selecting a pair of pseudo-peripheral (pseudo-diameter) nodes;

Phase 2: Nodal numbering.

In Phase 1, a pair of nodes is selected as starting and ending nodes according to the following steps:

Step 1: Choose an arbitrary node *s* of minimum degree;

Step 2: Generate the shortest route tree $SRT_s = \{C_1^s, C_2^s, \dots, C_d^s\}$ rooted in s. Let S be the list of the nodes of C_d^s , which is stored in the order of increasing degree;

Step 3: Decompose S into subsets S_j of cardinality $|S_j|$, $j = 1, 2, \dots, \Delta$, where Δ is the maximum degree of any node of S such that all nodes of S_j are characterized by degree j. Generate an SRT from each node y of S for the first $1 \leq m_j \leq \Delta$. If $d(\text{SRT}_y) > d(\text{SRT}_s)$, then set s = y and go to Step 2;

Step 4: Let e be the root of the longest SRT that has the smallest width. When the algorithm terminates, s and e are the end points of a pseudo-diameter.



Figure 1. Different statuses of nodes.

In Phase 2 the nodes of an element clique graph are reordered, and it is ensured that the position of a node in this reordering phase follows a priority rule according to the following steps:

Step 1: Find the status of all nodes. A node can be found in one status of the following cases, as shown in Figure 1. A node that has been assigned a new label is considered as *post-active*. Nodes that are adjacent to a post-active node, yet do not have a post-active status, are called *active*. Each node which is adjacent to an active node, but is not post-active or active, is said to be *pre-active*. The nodes which are not post-active, active, or pre-active are considered as *inactive*;

Step 2: Prepare a list of the candidate nodes, consisting of active and pre-active nodes, for labeling in the next step;

Step 3: Calculate the priority number of all the candidate nodes. For node i, the number is obtained from the following relationship:

$$P_i = W_1 \times \delta_i - W_2 \times D_i,\tag{4}$$

where W_1 and W_2 are integer weights (suggested as $W_1 = 1$ and $W_2 = 2$ in the original Sloan's algorithm), δ_i is the distance between each node *i* and the end node, and D_i is the incremental degree of node *i*, which is defined as follows:

$$D_i = d_i - c_i + k_i,\tag{5}$$

where d_i is the degree of node i, c_i is the number of active and post-active nodes adjacent to node i, and k_i is zero if node i is active or post-active, and unity otherwise;

Step 4: Select the node with the highest priority among the candidate nodes and label it;

Step 5: Repeat Steps 1-4 until all the nodes of the graph are labeled.

In Eq. (4) if $W_1 = 0$ and $W_2 = 1$, the node labeling algorithm becomes identical to the one proposed by King [8].

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2.3. The priority function with new integer weights

According to Eq. (4), a linear priority function of two graph parameters is employed in Sloan's algorithm, and the weights determine the rank of each parameter. Sloan has recommended the pair $W_1 = 1$ and $W_2 = 2$ for the weights. However, some research results show that, for some problems, using other values leads to better results.

The priority was generalized by Kaveh and Rahimi Bondarabdy [18] to a linear function of vectors of graph parameters as follows:

$$F_i = \sum_{i=1}^{L} W_i \times G_i, \tag{6}$$

where G_i $(i = 1, 2, \dots, L)$ are the normalized Ritz vectors representing the graph parameters, W_i $(i = 1, 2, \dots, L)$ are the weights of the Ritz vectors (Ritz coordinates), which are unknown. That is, one can utilize L characteristics of a graph to define the priority function and find the weights that can guide the algorithm to choose an optimal profile or wavefront.

L = 2 characteristics of the graph model are employed in Sloan's algorithm. Here, we find the best sets of weights for the priority function with L = 2 and 5. These sets of integer weights are found by utilizing PSO, CBO, ECBO, TWO, and VPS algorithms.

The method of L = 2 is presented as the first case. The vectors of graph properties are taken similar to those of Sloan's strategy. In the second case, the method of L = 5, which uses five vectors G_i $(i = 1, 2, \dots, 5)$, is presented as follows:

- G_1 : Degrees of the nodes;
- G_2 : The node distance from the end node;
- G_3 : The node distance from the starting node;
- G_4 : The 1-weighted degree;
- G_5 : The width of an SRT rooted in the starting node.

Once the vectors of graph parameters are formed, their weights can be obtained using PSO, CBO, ECBO, TWO, and VPS algorithms.

3. The utilized metaheuristic algorithms

Metaheuristic algorithms have been previously utilized to optimize the coefficients of the generalized Sloan function. Genetic algorithm [19], ant colony [20], charged system search [21], CBO, ECBO, and tug of war [22] are some of these applications. In this paper, VPS is added to the 3 algorithms used in the latter reference, and a more extensive comparison is made.

In this section, a brief description and pseudo codes of the colliding bodies optimization algorithm, its enhanced version, and then two new algorithms, called tug of War Optimization algorithm and vibrating particles system algorithm, are presented and employed to calculate the optimum values of the coefficients.

3.1. Colliding bodies optimization

The collision between two objects is a natural phenomenon. The colliding bodies optimization technique was developed based on this occurrence by Kaveh and Mahdavi [13]. In this technique, one object collides with another and, thus, they move towards a minimum energy level. CBO utilizes a simple formulation, does not employ memory for saving the best-so-far solutions, and requires no internal parameter. For further details, reader mays refer to [13]. The pseudo code of CBO is provided in Figure 2.

3.2. Enhanced colliding bodies optimization

Enhanced colliding bodies optimization is a modified version of CBO, which improves CBO to achieve highly reliable solutions, as was introduced by Kaveh and Ilchi Ghazaan [14]. The introduction of memory increases the convergence speed of ECBO more than that of CBO. Furthermore, changing some components of CBO helps ECBO escape local optima. For further



Figure 2. Pseudo code of the colliding bodies optimization algorithm.

Procedure Enhanced Colliding Bodies Optimization
for all CBs
Initial location is generated randomly
the value of objective function and mass are evaluated
end for
while termination condition is nor met (like max iteration)
Colliding Memory (CM) is updated
The population is updated
CBs are sorted according to their objective function values
for each CBs
Calculate CBs velocity before collision
Calculate CBs velocity after collision
New location is updated
if rand $i < Pro$
One dimension of the i th CB is selected randomly and regenerated
end if
end for
end while
end procedure

Figure 3. Pseudo code of the enhanced colliding bodies optimization algorithm.

Procedure Tug of War optimization						
Initialize parameters						
Initialize a population of N random candidate solutions						
Initialize the league by recording all random candidate solution						
while stop criteria is not attained						
Evaluate the objective function values for the candidate solutions						
Sort the new solutions and update the league						
Define the weights of the teams of the league W_i based on the fit(Xi)						
for each team i						
for each team j						
if $(W_i < W_j)$						
Move team i towards team j						
end if						
end for						
Determine the total displacement of team i						
Determine the final position of team i						
Use the side constraint handling technique to regenerate violating variables						
end for						
end while						
end procedure						

Figure 4. Pseudo code of the tug of war optimization algorithm.

details, readers may refer to [14]. The pseudo code of ECBO is provided in Figure 3.

3.3. Tug of War Optimization (TWO) algorithm

TWO is a population-based metaheuristic algorithm, which was introduced by Kaveh and Zolghadr [15]. This approach models each candidate solution $X_i = \{x_{i,j}\}$ as a team engaged in a series of tug of war competitions. The weight of the teams is determined based on the quality of the corresponding solutions, and the value of pulling force which a team can exert on the rope is assumed to be proportional to its weight. Naturally, the opposite team will have to maintain at least the same value of force in order to sustain its grip of the rope. The lighter team accelerates toward the heavier team, and this forms the convergence operator of TWO method. The method improves the quality of the solutions iteratively by keeping a proper exploration/exploitation balance and employing the described convergence operator. The pseudo code of TWO is provided in Figure 4.

3.4. Vibrating particles system algorithm

The vibrating particles system is a metaheuristic method and is inspired by the damped free vibration of single degree of freedom systems, as was introduced by Kaveh and Ilchi Ghazaan [16]. This approach involves a number of candidate solutions, representing the particles system. The particles are initialized randomly in an *n*-dimensional search space and gradually approach their equilibrium positions. To keep the balance between the exploration and exploitation, these equilibrium positions are achieved through the



Figure 5. Pseudo code of the vibrating particles system algorithm.

current population and the historically best position. The pseudo code of VPS is provided in Figure 5.

4. Numerical examples

In this section, eight Finite Element Meshes (FEMs) are considered. Element clique graph is a type of graph model that is employed for transferring topological properties of finite element models into connectivity properties of graphs [3]. The nodes of this graph model are the same as those of the corresponding finite element model with the nodes of each element being cliqued, and the multiple members in the entire graph are replaced by single members. Ten problems are presented to show the performance and efficiency of some new optimization algorithms. Four test problems are presented by Everstine [23]. The well-known standard PSO algorithm, two new algorithms, namely the colliding bodies optimization and enhanced colliding bodies optimization, and two recently developed methods called tug of war optimization and vibrating particles system are applied to reduce the profile and wavefront. The results of the reduction of profile and wavefront with L = 2 and 5 methods are compared with those of the Sloan and King's algorithms in Tables 1 to 16, respectively.

Example 1. A tower with 87 nodes and 227 elements is considered. The finite element mesh of this model is shown in Figure 6. The efficiency of the abovementioned algorithms is tested by this model for profile and wavefront reduction problems. The obtained results are given in Tables 1 and 2, respectively. The quality of the results is provided in these tables.

Example 2. The schematic of a finite element model of power supply housing is presented in Figure 7. This



Figure 6. Schematic of the FEM of a tower.



Figure 7. Schematic of the FEM of power supply housing.

model has 307 nodes and 1108 elements. The results of profile and wavefront reduction problems by employing optimization algorithms are given in Tables 3 and 4, respectively.

	Algorithm	No. of vectors	W_1	W_2	W_3	W_4	W_5	Profile
1, N = 87	Sloan		1	2				778
	King		0	1				795
	PSO	L = 2	0.1036	0.3706				767
		L = 5	-0.0144	-0.6110	0.7313	-0.0006	0.2632	571
	CBO	L = 2	0.2719	0.0641				692
		L = 5	-0.0589	-0.8641	0.9263	-0.0009	0.8139	571
ole	ECBO	L = 2	0.2830	0.8495				767
lme		L = 5	0.0217	-0.8665	0.9936	-0.0001	-0.0597	571
ΕX	TWO	L = 2	0.2707	0.9853				767
		L = 5	0.0011	-0.4868	0.5443	-0.0015	-0.9865	571
	VPS	L = 2	0.0640	0.2222				767
		L = 5	-0.0175	-0.7657	0.8836	-0.0001	0.8663	571

Table 1. Comparison of the results of profile reduction for the tower problem.

Table 2. Comparison of the results of wavefront reduction for the tower problem.

	Algorithm	No. of vectors	W_1	W_2	W_3	W_4	W_5	F_{rms}
	Sloan		1	2				8.7382
	King		0	1				9.2189
2	PSO	L = 2	0.2007	0.6255				9.6900
20 		L = 5	0.0009	-0.5316	0.5742	-0.0009	0.5547	6.9124
Z	CBO	L = 2	0.2875	0.8730				9.6900
1,		L = 5	0.0004	0.9800	-0.9047	-0.0008	0.3827	6.9124
ple	ECBO	L = 2	0.2428	0.8169				9.6900
am		L = 5	0.0005	-0.8408	0.9966	-0.0027	0.1399	6.9124
Εx	TWO	L = 2	0.2727	0.9664				9.6900
		L = 5	-0.1069	-0.6872	0.6581	-0.0040	0.8902	7.3085
	VPS	L = 2	0.0694	0.2674				9.6900
		L = 5	0.0000	-0.7642	0.9004	-0.0022	0.0390	6.9124



Figure 8. Schematic of the hull w/refinement model.

Example 3. A hull w/refinement model containing 310 nodes and 1069 elements is considered in Figure 8. Tables 5 and 6 provide the values of the profile and wavefront reduction, respectively, and the results can be compared with those of these tables.



Figure 9. FEM of a barge.

Example 4. The FEM of a barge with 419 nodes and 1579 elements is considered, as shown in Figure 9. Tables 7 and 8 provide the comparison results of profile and wavefront reduction problems by utilizing PSO, CBO, ECBO, TWO, and VPS algorithms for this example.

Example 5. A Z-shaped finite element model of a

	Algorithm	No. of vectors	W_1	W_2	W_3	W_4	W_5	Profile
	Sloan		1	2				8730
	King		0	1				9095
N-	PSO	L = 2	0.0042	0.2228				8205
307		L = 5	-0.0742	0.6049	-0.0674	0.0103	-0.5000	8421
N =	CBO	L = 2	0.0850	0.8204				8148
		L = 5	0.0174	-0.2591	0.9308	-0.0035	0.1450	8262
le 2	ECBO	L = 2	0.0546	0.9436				8205
ump		L = 5	-0.0035	-0.0601	0.3642	-0.0010	-0.9357	8262
EX3	TWO	L = 2	0.0248	0.3105				8189
		L = 5	-0.5751	-0.8167	-0.1357	-0.5099	0.6424	8004
	VPS	L = 2	0.0168	0.2476				8205
		L = 5	0.0009	-0.1628	0.9542	-0.0002	0.7594	8213

Table 3. Comparison of the results of profile reduction for the power supply housing problem.

Table 4. Comparison of the results of wavefront reduction for the power supply housing problem.

	Algorithm	No. of vectors	W_1	W_2	W_3	W_4	W_5	F_{rms}
	Sloan		1	2				31.2292
	King		0	1				32.0931
~	PSO	L = 2	0.1578	0.9402				27.5724
307		L = 5	0.0105	0.1509	-0.9033	-0.0056	-0.6496	30.5202
/	CBO	L = 2	0.1641	0.7762				30.6501
4		L = 5	-0.0375	-0.1102	0.9901	0.0056	-0.0212	28.426
le 1	ECBO	L = 2	0.0777	0.9292				27.6011
ump		L = 5	-0.0416	-0.0428	0.9934	0.0080	-0.0424	28.4111
Exa	TWO	L = 2	0.0069	0.0459				27.2907
		L = 5	-0.3605	-0.9187	-0.0700	-0.7603	-0.7260	27.2771
	VPS	L = 2	0.0368	0.7499				27.2907
		L = 5	0.0042	-0.0490	0.8914	-0.0011	-0.3126	27.7194

	Algorithm	No. of vectors	W_1	W_2	W_3	W_4	W_5	Profile
	Sloan		1	2				3211
310	King		0	1				3222
	PSO	L = 2	0.4576	0.1340				3171
		L = 5	-0.0317	0.5209	-0.3798	-0.0137	0.9275	3170
	CBO	L = 2	0.9282	0.2813				3171
~		L = 5	0.0290	0.3456	0.9489	-0.0134	0.3580	3125
le	ECBO	L = 2	0.9380	0.2136				3179
du		L = 5	-0.0108	-0.1277	0.8426	-0.0031	0.1786	3125
Jxa	TWO	L = 2	0.9556	0.3112				3179
		L = 5	0.4208	-0.9040	-0.8360	-0.9611	0.6841	2979
	VPS	L = 2	0.1361	0.0405				3171
		L = 5	-0.0368	-0.1685	0.9088	-0.0012	-0.8294	3125

	Algorithm	No. of vectors	W_1	W_2	W_3	W_4	W_5	F_{rms}
Example 3, $N = 310$	Sloan		1	2				10.5232
	King		0	1				10.5841
0	PSO	L = 2	0.4899	0.1379				10.4361
310		L = 5	0.0326	-0.1466	0.7705	-0.0080	0.2158	10.2531
	CBO	L = 2	0.8400	0.2420				10.4108
с Э		L = 5	0.0115	-0.0681	0.4104	-0.0024	0.0422	10.2716
ole	ECBO	L = 2	0.8420	0.8420				10.4108
am]		L = 5	-0.0502	-0.1924	0.8743	-0.0003	0.4107	10.2716
Εx	TWO	L = 2	0.9624	0.2722				10.4108
		L = 5	-0.7532	-0.6871	-0.6053	-0.9134	-0.0993	9.7714
	VPS	L = 2	0.5418	0.1575				10.4361
		L = 5	-0.0307	-0.1404	0.8417	-0.0008	0.2558	10.2716

Table 6. Comparison of the results of wavefront reduction for the refined finite element model.

 Table 7. Comparison of the results of profile reduction for the barge problem.

	Algorithm	No. of vectors	W_1	W_2	W_3	W_4	W_5	$\mathbf{Profile}$
	Sloan		1	2				9113
	King		0	1				9301
6	PSO	L = 2	0.5179	0.0881				8808
: 41		L = 5	-0.0932	-0.2695	0.7979	0.0075	0.4298	8651
	CBO	L = 2	0.7913	0.1417				8808
Ľ,		L = 5	-0.1436	-0.2777	0.9433	0.0140	0.2705	8646
le 4	ECBO	L = 2	0.8527	0.1544				8802
du		L = 5	-0.9124	0.4662	-0.7636	-0.0054	-0.0497	8640
Jxa	TWO	L = 2	0.9766	0.1637				8804
		L = 5	0.0331	0.9569	-0.1261	-0.0064	0.9825	8643
	VPS	L = 2	0.3376	0.0664				8804
		L = 5	0.0287	-0.2435	0.9158	-0.0092	-0.1923	8630

Table 8. Comparison of the results of wavefront reduction for the barge problem.

	Algorithm	No. of vectors	W_1	W_2	W_3	W_4	W_5	F_{rms}
	Sloan		1	2				22.5524
	King		0	1				23.0926
6	PSO	L = 2	0.7145	0.1413				21.6733
: 41		L = 5	0.1294	0.7287	-0.2671	-0.0203	-0.2336	21.3466
 >	CBO	L = 2	0.9711	0.1722				21.6906
<u>к</u>		L = 5	-0.0756	0.8504	-0.2259	0.0063	-0.6770	21.2456
le 4	ECBO	L = 2	0.2526	0.0449				21.6583
du		L = 5	-0.0531	-0.2415	0.9790	0.0044	-0.0757	21.2783
Зха	TWO	L = 2	0.4787	0.0870				21.6733
		L = 5	-0.0402	0.9657	-0.3727	0.0033	0.8098	21.2683
	VPS	L = 2	0.3065	0.0611				21.6593
		L = 5	-0.1294	0.9687	-0.3533	0.0105	-0.7296	21.2456



Figure 10. FEM of a shear wall.



Figure 11. The element clique graph of a rectangular FEM with four openings.

shear wall with 550 nodes is considered. The element clique graph of this model is shown in Figure 10. The performance of the algorithms is tested by this model for profile and wavefront reduction problems. The results are given in Tables 9 and 10, respectively.

Example 6. The element clique graph of a rectangular FEM with four openings, as shown in Figure 11, contains 760 nodes. The performances of PSO, CBO, ECBO, TWO, and VPS algorithms are tested by this model for profile and wavefront reduction problems. The results for these problems are represented in Tables 11 and 12, respectively.

Example 7. The grid model of a fan with 1 D beam elements containing 1575 nodes is considered, as shown in Figure 12. Similar to the previous examples, the obtained values by the algorithms for profile and wavefront reduction problems are given in Tables 13 and 14, respectively, where the results can easily be compared.



Figure 12. The graph model of a fan.



Figure 13. Finite element grid model of a shear wall.

Example 8. The graph model of an H-shaped shear wall with 4949 nodes is considered, as shown in Figure 13. The performance of the above-mentioned algorithms is verified by this model, and the results of these algorithms for profile and wavefront reduction problems are provided in Tables 15 and 16, respectively.

5. Concluding remarks

The main aim of this study is to use VPS algorithm for profile and wavefront reduction of finite element mesh matrices for the first time and to present the pseudo codes for CBO, ECBO, TWO, and VPS algorithms. The results of these algorithms, when applied to 8 real-life finite element models, were then compared. According to Tables 1 to 16, it can be observed that the achieved results of these algorithms were quite satisfactory, compared to the well-known graph theoretical method of the King and Sloan.

	Algorithm	No. of vectors	W_1	W_2	W_3	W_4	W_5	Profile
	Sloan							10530
	King							10974
0	PSO	L = 2	0.0007	0.4852				10501
550		L = 5	-0.0863	0.4638	-0.3677	0.0034	0.9191	9280
	CBO	L = 2	0.0043	0.4001				10501
2		L = 5	0.2191	0.9551	-0.6962	-0.0390	-0.3207	9242
ole a	ECBO	L = 2	0.0001	0.9881				10501
ump		L = 5	-0.0255	0.8883	-0.6256	-0.0110	-0.9183	9237
Εxε	TWO	L = 2	0.0129	0.7645				10501
		L = 5	-0.0404	0.8801	-0.5940	-0.0063	0.7426	9237
	VPS	L = 2	0.0024	0.4913				10501
		L = 5	-0.0917	0.9658	-0.6458	-0.0017	0.2137	9237

Table 9. Comparison of the results of profile reduction for the shear wall problem.

Table 10. Comparison of the results of wavefront reduction for the shear wall problem.

	Algorithm	No. of vectors	W_1	W_2	W_3	W_4	W_5	F_{rms}
	Sloan							20.1739
N = 550	King							21.0798
	PSO	L = 2	0.3069	0.2202				20.1401
		L = 5	-0.3188	0.9852	-0.7009	0.0489	0.118	17.2693
	CBO	L = 2	0.8701	0.6144				20.1401
		L = 5	-0.1888	0.9093	-0.8122	0.0210	0.8648	17.1544
le l	ECBO	L = 2	0.8858	0.6517				20.1401
amp		L = 5	-0.1891	-0.8720	0.9777	0.0199	-0.4653	17.2239
Εx:	TWO	L = 2	0.8711	0.6352				20.1401
		L = 5	0.0101	0.9086	-0.8164	-0.0034	-0.1742	17.1492
	VPS	L = 2	0.2634	0.1834				20.1401
		L = 5	-0.2682	-0.8807	0.8722	-0.0001	0.5653	17.2057

Table 11.	Comparison	of the	results of	profile	reduction	for the	rectangular	FEM	with a	a four-	opening	problem.
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	Algorithm	No. of vectors	W_1	W_2	W_3	W_4	W_5	Profile
	Sloan							18719
	King							18839
0	PSO	L = 2	0.6645	0.9066				18690
- 76		L = 5	0.1056	0.8858	-0.4835	-0.0152	0.0524	17136
	CBO	L = 2	0.1899	0.2566				18689
3, 7		L = 5	-0.3332	-0.7097	0.9412	0.0507	0.9747	17122
le (ECBO	L = 2	0.6665	0.9228				18581
du		L = 5	-0.0458	0.7835	-0.6332	0.0060	-0.2254	17039
Jxa	TWO	L = 2	0.7136	0.9633				18581
H		L = 5	-0.0178	-0.4092	0.9291	0.0024	-0.5575	17039
	VPS	L = 2	0.1785	0.2491				18581
		L = 5	-0.0513	0.796	-0.3421	0.007	0.0739	17039

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	Algorithm	No. of vectors	W_1	W_2	W_3	W_4	W_5	F_{rms}
	Sloan							25.9092
	King							26.6508
0	PSO	L = 2	0.2053	0.3469				25.8411
76(L = 5	-0.0879	-0.3811	0.8933	0.012	-0.1249	23.5891
	CBO	L = 2	0.3181	0.5433				25.8438
N N		L = 5	-0.0713	-0.6558	0.9556	0.0095	-0.6861	23.4955
le (ECBO	L = 2	0.1855	0.3155				25.8411
dun		L = 5	-0.1056	0.8982	-0.7698	0.0121	-0.7255	23.4743
Ex	TWO	L = 2	0.5752	0.9624				25.8438
		L = 5	-0.0919	0.9571	-0.6803	0.0130	-0.0568	23.5090
	VPS	L = 2	0.0287	0.05				25.8438
		L = 5	-0.0622	-0.4264	0.9926	0.0086	-0.2518	23.4599

Table 12. Comparison of the results of wavefront reduction for the rectangular with a four-opening problem.

Table 13. Comparison of the results of profile reduction for the fan model.

	Algorithm	No. of vectors	W_1	W_2	W_3	W_4	W_5	Profile
	Sloan							28703
1575	King							28853
	PSO	L = 2	0.2588	0.6068				28629
		L = 5	-0.2965	0.5407	-0.6326	-0.0214	-0.1835	29674
	CBO	L = 2	0.2129	0.4426				28608
e 7, N		L = 5	-0.5700	0.8618	-0.5831	0.0777	0.3363	27992
	ECBO	L = 2	0.1765	0.9272				28587
mpl		L = 5	-0.4186	0.9776	-0.7792	0.1007	-0.0557	27982
Bxa	TWO	L = 2	0.1613	0.8465				28579
-		L = 5	-0.3306	0.8144	-0.5654	0.0668	0.6810	27977
	VPS	L = 2	0.0274	0.1543				28568
		L = 5	-0.6613	0.8839	-0.637	0.149	-0.2288	27982

Table 1	14.	Comparison	of	the	results	of	wavefront	reduction	for	$_{\mathrm{the}}$	$_{\mathrm{fan}}$	model.
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	Algorithm	No. of vectors	W_1	W_2	W_3	W_4	W_5	F_{rms}
	Sloan							18.3958
1575	King							18.4698
	PSO	L = 2	0.0605	0.3289				18.3126
		L = 5	-0.0709	0.6589	-0.9003	-0.0677	-0.4860	18.9964
	CBO	L = 2	0.1382	0.8659				18.3235
Z,		L = 5	-0.2174	-0.4203	0.4590	0.0462	-0.2162	19.2531
e 7	ECBO	L = 2	0.1688	0.8892				18.3232
lqn		L = 5	0.1883	0.7370	-0.5928	-0.0607	-0.0945	18.6574
xaı	TWO	L = 2	0.0357	0.1982				18.3240
E		L = 5	0.0441	0.9101	-0.7696	0.0139	-0.6153	18.0211
	VPS	L = 2	0.0597	0.3524				18.3168
		L = 5	-0.2561	-0.3969	0.5031	0.0699	-0.7877	18.2694

		1		1				
	Algorithm	No. of vectors	W_1	W_2	W_3	W_4	W_5	$\mathbf{Profile}$
	Sloan							157457
	King							157103
49	PSO	L = 2	0.0449	0.6963				157095
49		L = 5	0.1106	0.9323	-0.0624	-0.0284	-0.3706	160705
N =	CBO	L = 2	0.0229	0.9146				157095
		L = 5	-0.9709	-0.9856	0.1853	0.2102	-0.3565	159681
e So	ECBO	L = 2	0.0620	0.9365				157095
lqn		L = 5	-0.5805	-0.7778	0.2437	0.1277	-0.1065	159676
xaı	TWO	L = 2	0.0721	0.9800				157095
Ŧ		L = 5	-0.8206	-0.8691	0.5953	0.4801	0.2781	159675
	VPS	L = 2	0.0081	0.8161				157095
		L = 5	-0.8685	-0.9894	0.0888	0.1738	-0.1293	159638

 Table 15. Comparison of the results of profile reduction for the H-shape problem.

Table 16. Comparison of the results of wavefront reduction for the H-shape problem.

	Algorithm	No. of vectors	W_1	W_2	W_3	W_4	W_5	F_{rms}
	Sloan							32.3665
	King							32.2875
1 9	PSO	L = 2	0.0445	0.6963				32.2869
49		L = 5	0.2036	-0.9340	0.0601	0.0151	-0.5008	32.9486
	CBO	L = 2	0.0361	0.8204				32.2869
N,		L = 5	-0.0469	-0.9805	0.0890	0.0109	-0.0406	32.7939
e ø	ECBO	L = 2	0.0145	0.6215				32.2869
ldu		L = 5	-0.0665	-0.9779	0.2937	0.0204	0.0726	32.8298
xar	TWO	L = 2	0.0772	0.9898				32.2869
£		L = 5	-0.3335	-0.6943	0.6808	0.1610	-0.0604	32.8845
	VPS	L = 2	0.0025	0.3597				32.2869
		L = 5	-0.6995	-0.8788	0.0746	0.1439	0.8584	32.7883

In profile and wavefront reduction problems with L = 2 and 5 methods, an attempt was made to display the applicability of using different priority functions by utilizing CBO, ECBO, TWO, and VPS algorithms. Optimal weights for these functions were achieved in the optimization processes for reducing the profile and wavefront of the stiffness matrices of the finite element models. According to Tables 1 to 16, it can be observed that Sloan and King's approaches can improve in most cases using some new parameters and weights. The weights obtained for different examples show that, compared to Sloan and King's algorithms, more suitable profile and wavefront values can be achieved by using the two-parameter method (L = 2). Compared to the two-parameter method and Sloan and King's algorithms, smaller profile and wavefront values can be attained in the five-parameter scheme (L = 5). However, for Example 8, the values of profile and wavefront of the Sloan and King's methods are smaller than those of the five-parameter algorithm. It should be noted that, in L = 5 approach, the active degrees are not updated as in Sloan's technique. Therefore, one should not always expect a better result when five adjusted parameters are employed instead of two free parameters. Since the graph properties employed in L = 5 method are more than those in L = 2 approach, the amount of reduction in profile and wavefront is higher than that in the Sloan and King's algorithms. The comparison results of the profile and wavefront reduction problem for Example 4 are shown in Figures 14 and 15, respectively.

The new recently developed metaheuristic algorithm, namely the vibrating particles system, has been employed in this study for the first time. Tables 1 to 16 demonstrate that this algorithm finds superior optimal values for profile and wavefront of most of the investigated problems. Moreover, the optimized results obtained by TWO and VPS can compete in performance with those obtained by the other three optimization methods of PSO, CBO, and ECBO and



Figure 14. Comparison of profile results for Example 4.



Figure 15. Comparison of the wavefront results for Example 4.



Figure 16. Convergence curves obtained for Example 4.

attain better results in some cases. Figures 16-17 and Figures 18-19 show the convergence rate comparisons of these algorithms for profile and wavefront reduction in the case of Examples 4 and 6, respectively.

It should be mentioned that the optimization proposed in this paper was performed to improve the coefficients of Sloan's algorithm and was not necessarily limited to the profile reduction of sparse matrices. A direct optimization may or may not result in better values for the profile of the models.

Although the methods of this paper are used for nodal ordering in the stiffness method, their application



Figure 17. Convergence curves obtained for Example 4.



Figure 18. Convergence curves obtained for Example 6.



Figure 19. Convergence curves obtained for Example 6.

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can easily be extended to ordering the self-equilibrating systems in the force method.

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Biographies

Ali Kaveh was born in 1948 in Tabriz, Iran. After graduation from the Department of Civil Engineering at the University of Tabriz in 1969, he continued his studies on Structures at Imperial College of Science and Technology at London University and received his MSc, DIC, and PhD degrees in 1970 and 1974, respectively. He then joined the Iran University of Science and Technology. Professor Kaveh is the author of 625 papers published in international journals and 155 papers presented at national and international conferences. He has authored 23 books in Farsi and 8 books in English published by Wiley, RSP, American Mechanical Society, and Springer.

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